



## Planck 2013 results. VII. HFI time response and beams

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# Planck 2013 results. VII. HFI time response and beams

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## ABSTRACT

This paper characterizes the *effective beams*, the *effective beam window functions* and the associated errors for the *Planck* High Frequency Instrument (HFI) detectors. The effective beam is the angular response including the effect of the optics, detectors, data processing and the scan strategy. The window function is the representation of this beam in the harmonic domain that is required to recover an unbiased measurement of the Cosmic Microwave Background (CMB) angular power spectrum. The HFI is a scanning instrument and its effective beams are the convolution of (a) the optical response of the telescope and feeds, (b) the processing of the time ordered data and deconvolution of the bolometric and electronic transfer function, and (c) the merging of several surveys to produce maps. The time response transfer functions are measured using observations of Jupiter and Saturn and by minimizing survey difference residuals. The *scanning beam* is the post-deconvolution angular response of the instrument, and is characterized with observations of Mars. The main beam solid angles are determined to better than 0.5% at each HFI frequency band. Observations of Jupiter and Saturn limit near sidelobes (within 5°) to ~ 0.1% of the total solid angle. Time response residuals remain as long tails in the scanning beams, but contribute less than 0.1% of the total solid angle. The bias and uncertainty in the beam products are estimated using ensembles of simulated planet observations that include the impact of instrumental noise and known systematic effects. The correlation structure of these ensembles is well-described by five error eigenmodes that are sub-dominant to sample variance and instrumental noise in the harmonic domain. A suite of consistency tests provide confidence that the error model represents a sufficient description of the data. The total error in the effective beam window functions is below 1% at 100 GHz up to multipole  $\ell \sim 1500$ , and below 0.5% at 143 and 217 GHz up to  $\ell \sim 2000$ .

**Key words.** Cosmology: observations – Cosmic background radiation – Surveys – Space vehicles: instruments – Instrumentation: detectors

## 1. Introduction

This paper, one of a set associated with the 2013 release of data from the *Planck*<sup>1</sup> mission (Planck Collaboration I 2013), de-

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scribes the impact of the optical system, detector response, analog and digital filtering and the scan strategy on the determination of the HFI angular power spectra. An accurate understanding of this response, and the corresponding errors, is necessary in order to extract astrophysical and cosmological information from CMB data (Hill et al. 2009; Nolte et al. 2009; Huffenberger et al. 2010).

Bolometers, such as those used in the HFI on *Planck*, are phonon-mediated thermal detectors with finite response time to changes in the absorbed optical power. The observations are affected by attenuation and phase shift of the signal resulting from a detector's thermal response as well as the analog and digital filtering in the associated electronics.

In the small signal regime (appropriate for CMB fluctuations and the Galactic emission), the receiver response can be well approximated by a complex Fourier domain transfer function, termed the *time response*. The time-ordered data (also referred to as time-ordered information, or TOI) are approximately deconvolved by the time response function prior to calibration and map-making (for recent examples of CMB observations with similar semiconductor bolometers see Tristram et al. (2005) and Masi et al. (2006)).

Ideally, the deconvolved TOIs represent the true sky signal convolved by the optical response of the telescope (or *physical beam*) and filtered by the TOI processing. The combination of the time domain processing and the physical beam convolution is, in practice, degenerate due to the nature of the scan strategy; the *Planck* spacecraft scans at 1 rpm with variations less than 0.1 % (Planck Collaboration I 2011). The beams reconstructed from the deconvolved planetary observations are referred to as the *scanning beam*.

These deconvolved data are then projected into a pixelized map, as discussed in Sect. 6. of Planck Collaboration VI (2013). To a good approximation, the effect of the map-making algorithm is to average the beam over the observed locations in a given pixel. This average is referred to as the *effective beam*, which will vary from pixel to pixel across the sky. The map-making procedure implicitly ignores any smearing of the input TOIs; no attempt is made to deconvolve the optical beam and any remaining electronic time response. Thus, any further use of the resulting maps must take into account the effective beam.

To obtain an unbiased estimate of the angular power spectrum of the CMB, one must determine the impact of this effective beam pattern on a measurement of an isotropic Gaussian random signal in multipole ( $\ell$ ) space. The filtering effect is well approximated by a multiplicative *effective beam window function*, derived by coupling the scan history with the scanning beam profile, that is used to relate the angular power spectrum of the map to that of the underlying sky (Hivon et al. 2002).

The solar and orbital motion of *Planck* with respect to the surface of last scattering provides a 60-second periodic signal in the time ordered data that is used as a primary calibrator. This normalizes the window function at a multipole  $\ell = 1$ ; the effective beam window function is required to transfer this calibration to smaller angular scales.

These successive products (the scanning beam, the effective beam and the effective beam window function) must be accompanied by an account of their errors, which are characterised through ensembles of dedicated simulations of the planetary ob-

servations. The error on the effective beam window function is found to be sub-dominant to other errors in the cosmological parameter analysis (Planck Collaboration XVI 2013).

The scanning beam is thus measured with on-orbit planetary data, coupling the response of the optical system to the deconvolved time response function and additional filters in the TOI processing. As shown in the following, the main effect of residual deconvolution errors is a bias in the beam window function of order  $10^{-4}$  at  $\ell > 100$  due to a residual tail in the beam along the scan direction.

The scanning beam can be further separated into the following components:

1. The main beam, which is defined as extending to  $30'$  from the beam centroid.
2. The near sidelobes, which extend between  $30'$  and  $5^\circ$ . These are typically features below  $-30$  dB, and include the optical effects of phase errors, including both random and periodic surface errors and residuals due to the imperfect deconvolution of the time response.
3. The far sidelobes, which extend beyond  $5^\circ$ . These features are dominated by spillover, namely power coupling from the sky to the feed antennas directly, or via a single reflection around the mirrors and baffles. The minimum in the beam response between the main beam and direct spillover of the feed over the top of the secondary mirror falls at roughly  $5^\circ$ , making such a division natural (Tauber et al. 2010).

This paper describes the main beam and the near sidelobes, the resulting effective beam patterns on the sky and the effective beam window function used for the measurement of angular power spectra, along with their errors. The effects of the far sidelobes are mainly discussed in Planck Collaboration VI (2013) and Planck Collaboration XIV (2013), their effects on calibration described in Planck Collaboration X (2013). A companion paper (Planck Collaboration IV 2013) computes the effective beams and window functions for *Planck*'s Low Frequency Instrument (LFI). Despite using very different methods that depend more strongly on optical modelling, these instruments produce compatible power spectra, providing a cross-check of both approaches (Planck Collaboration XI 2013).

The signal to noise ratio of Jupiter observations with HFI allows the measurement of near sidelobes to a noise floor of  $-45(-55)$  dB at 100 (857) GHz. The HFI analysis does not rely on a physical optics model to constrain the behaviour of the beam in this regime.

On-orbit measurements of the *Planck* HFI scanning beam and temporal transfer function have been previously reported in Planck HFI Core Team (2011a) for the Early Release Compact Source Catalog (ERCSC; Planck Collaboration VII (2011)) and early science from *Planck*. Section 2 presents an improved model for the time response and explains how its parameters are derived using on-orbit data and how it is deconvolved from the data. Figure 1 provides a flowchart of the determination of the time response parameters. Figure 2 is the flowchart of the steps that lead from planet measurements to effective beams, effective beam window functions and assessment of uncertainties. Section 3 describes how the scanning beams are reconstructed from planet observations. Section 3.4 describes the effects of long time scale residuals in the data due to imperfect deconvolution of the time response. Section 4 describes the propagation of the scanning beams to effective beams and effective beam window functions using the scanning history of *Planck*. Section 5 describes the techniques used to propagate statistical and systematic errors and to check the consistency of the beams and

states (in particular the lead countries: France and Italy) with contributions from NASA (USA), and telescope reflectors provided in a collaboration between ESA and a scientific Consortium led and funded by Denmark.

window functions. Section 6 describes the final error budget and the eigenmode decomposition of the errors in the effective beam window function.

## 2. Time Response

In *Planck*'s early data release, a 10-parameter model TF10 describes the time response of the bolometer/electronics system (Planck HFI Core Team 2011a). This section describes an improved model of the time response based on the HFI readout electronics schematics that more accurately reproduces phase shifts in the system close to the Nyquist frequency. The improved model also provides more degrees of freedom for the bolometer's thermal response in order to describe more accurately the low frequency response of the bolometer.

### 2.1. Model

The new model is named LFER4 (Low Frequency Excess Response with 4 time constants) and consists of an analytic model of HFI's readout electronics (Lamarre et al. 2010) and 4 thermal time constants and associated amplitudes for the bolometer:

$$TF(\omega) = F(\omega)H'(\omega; S_{\text{phase}}, \tau_{\text{stray}}), \quad (1)$$

where  $TF(\omega)$  represents the full time response as a function of angular frequency  $\omega$ . The time response of the bolometer alone is modeled by

$$F(\omega) = \sum_{i=1,4} \frac{a_i}{1 + i\omega\tau_i}, \quad (2)$$

and  $H'(\omega; S_{\text{phase}}, \tau_{\text{stray}})$  is the analytic model of the electronics transfer function (whose detailed equations and parameters are given in Appendix A) with two parameters.

The overall normalization of the transfer function is forced to be 1.0 at the signal frequency of the dipole, leaving a total of 9 free parameters for each bolometer.

The sum of single-pole low-pass filters represents a lumped-element thermal model with four elements. The thermal model underlying the temporal transfer function is described elsewhere (Spencer 2013); this work adopts an empirical approach to correcting the data.

The two parameters of  $H'$  mainly affect the high frequency portion of the time response.  $S_{\text{phase}}$  represents the phase difference between the bias and the lock-in summation, and is fixed in the model as a readout electronics setting. The second parameter  $\tau_{\text{stray}}$  is the time constant of the bolometer resistance and the parasitic capacitance of the wiring and is measured independently during the CPV phase of the mission. All resistance and capacitance values of the readout electronics chain are fixed at values from the circuit diagram.

The in-flight data are used to determine the remaining seven free parameters. Planetary observations are used to constrain those parameters governing the high frequency portion of the time response, while the low frequency parameters are constrained by minimizing the difference between the first and second survey maps.

The fastest thermal time constants in the LFER4 model roughly correspond to the time constants measured during pre-launch tests of the bolometers (Holmes et al. 2008; Pajot et al. 2010). The slower time constants contribute lower frequency response at the several percent level. The time constants in the LFER4 model are not exactly identical to those measured on

glitches (Planck Collaboration X 2013) due to additional filtering applied by the deglitching. A future publication (Spencer 2013) will relate the time constants and amplitudes to the thermal properties of the bolometer and module.

### 2.2. Fitting slow time constants with galaxy residuals

As *Planck* scans across the Galactic plane, the low frequency time response of HFI spreads Galactic signal away from the plane. Surveys 1 and 2 consist of roughly six months of data each and cover nearly the same sky, scanned at almost opposite angles. The difference between maps made with data from the two individual surveys highlights the effect since the Galactic power is spread in different directions in the two surveys, creating symmetric positive and negative residuals in the difference map. The LFER4 parameters are varied to minimize the difference between these surveys. In most cases, the fit is limited to the slowest time constant and its associated amplitude, and in others the fit is extended to the two slowest time constants and associated amplitudes.

Other systematic effects can confuse the measurement of LFER4 parameters by creating a similar positive/negative residual pattern in the survey difference. The philosophy employed here is to minimize the survey residuals fitting only for LFER4 parameters, but to use simulations and data selections to test the dependency of the results with other systematics.

#### 2.2.1. Survey difference method 1

Two techniques are used to perform the fit. The first method is based on map re-sampling in the time domain, using the pointing to generate synthetic TOI. The synthetic TOI of each survey is compared with the synthetic TOI of both surveys combined. Before the production of these synthetic TOI, the maps are smoothed to 30'. Given the fact that in consecutive surveys the scan direction is nearly opposite, the survey 2 TOI is very similar to the *time-reversal* of the survey 1 TOI. This symmetry is assumed to be exact, ensuring that time reversal is equivalent to taking the complex conjugate in the frequency domain. Since the sky signal has been convolved by the true transfer function,  $TF_{\text{true}}(\omega)$ , and deconvolved by the estimated – not fully correct – transfer function  $TF_0(\omega)$ , the single survey re-sampled time-stream is

$$d_1(t) = \mathcal{F}^{-1}(TF_{\text{true}}(\omega)/TF_0(\omega) \otimes \mathcal{F}(s(t'))), \quad (3)$$

where  $\mathcal{F}$  is the Fourier operator,  $s$  is the true sky map observed at time  $t'$ , and  $d_1$  is the synthetic TOI. This can be written as,

$$d_1(t) = \mathcal{F}^{-1}(\delta TF(\omega) \otimes \mathcal{F}(s(t'))), \quad (4)$$

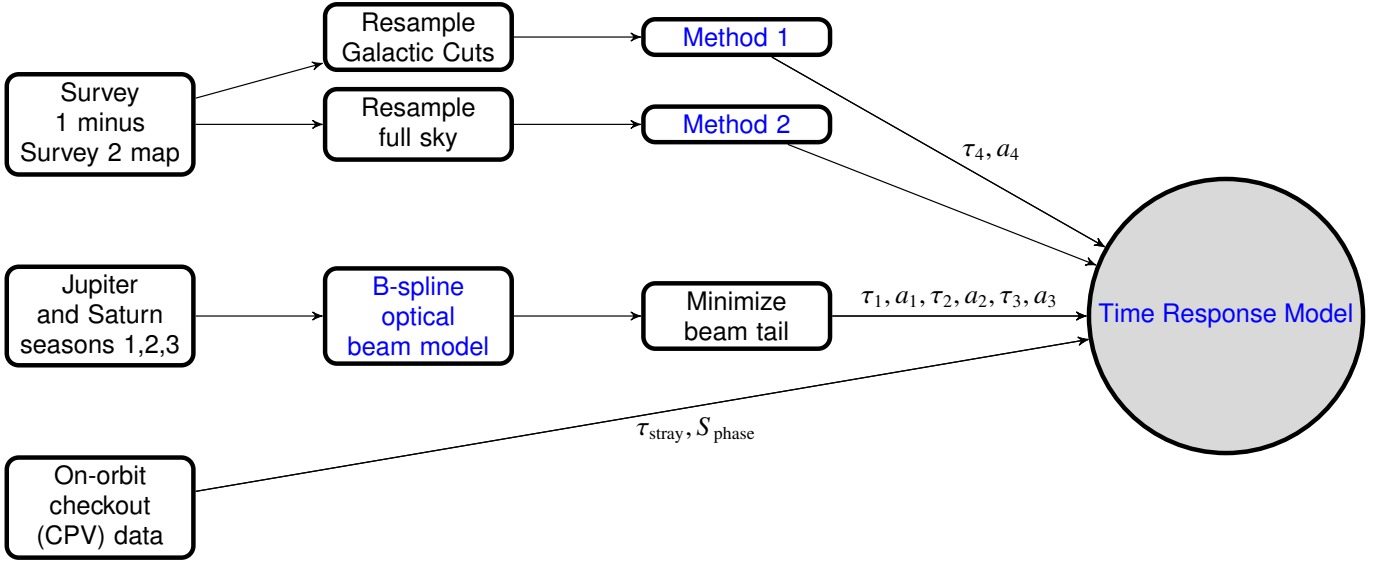
having defined  $\delta TF(\omega) = TF_{\text{true}}(\omega)/TF_0(\omega)$  as the corrective factor which should be applied to the estimated transfer function. The synthetic TOI of survey 2,  $d_2$ , is similarly defined. For the TOI of both surveys combined, the average of the two maps is used.

Using the property of the time reversal recalled above, the synthetic TOI  $d(t)$  of the full sky map (survey 1 and survey 2 combined) may be written as

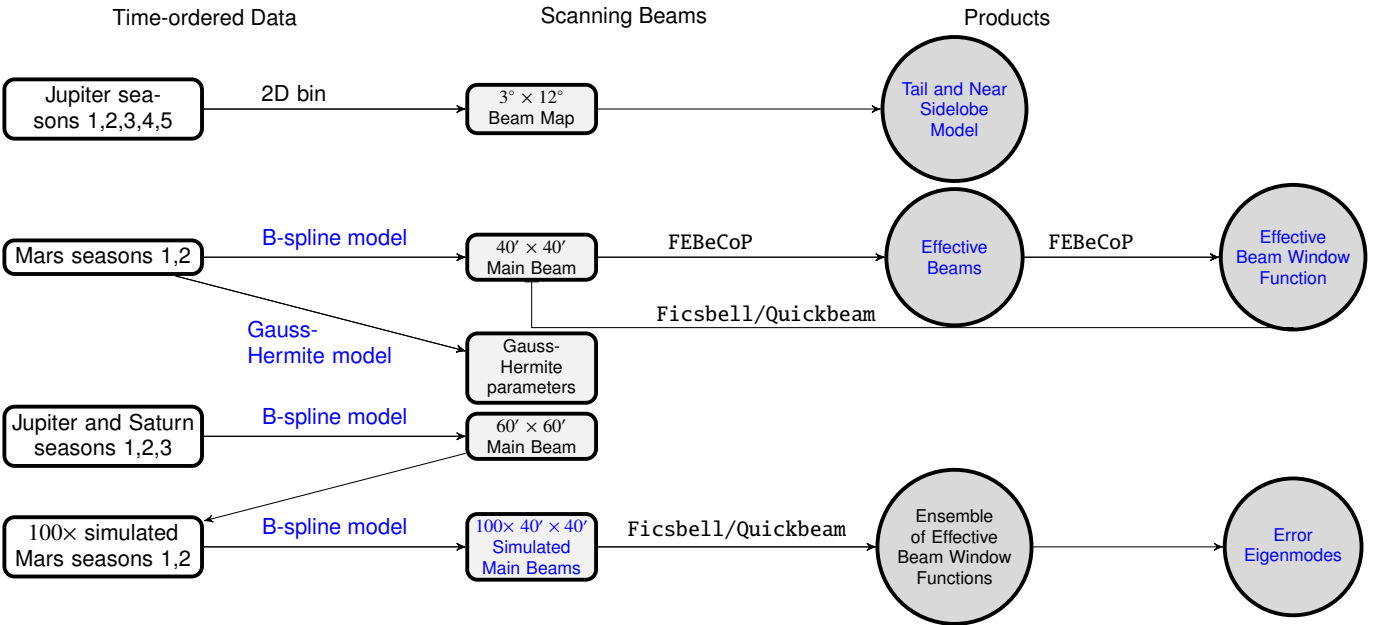
$$d(t) = \mathcal{F}^{-1} \left( \frac{\delta TF(\omega) + \delta TF^*(\omega)}{2} \otimes \mathcal{F}(s(t')) \right).$$

In Fourier domain, the ratio of the TOIs is

$$R(\omega) = \frac{\mathcal{F}(d_1(t))}{\mathcal{F}(d(t))} = \frac{\delta TF(\omega)}{\Re(\delta TF(\omega))} = 1 + j \frac{\Im(\delta TF(\omega))}{\Re(\delta TF(\omega))}.$$



**Fig. 1.** Data flow for fitting time response model parameters.



**Fig. 2.** Data flow for determining HFI's beams.

Since the real part of the transfer function at low frequency is close to 1, the imaginary part of the ratio of the synthetic beams is equal to the imaginary part of the corrective factor,  $\delta\text{TF}(\omega)$ :

$$\Im(R) = \Im(\delta\text{TF}(\omega)).$$

The LFER4 model of the transfer function is fitted to this measure of the imaginary part of the correction to infer the parameters of the true transfer function, in the low frequency regime, typically below a few Hz.

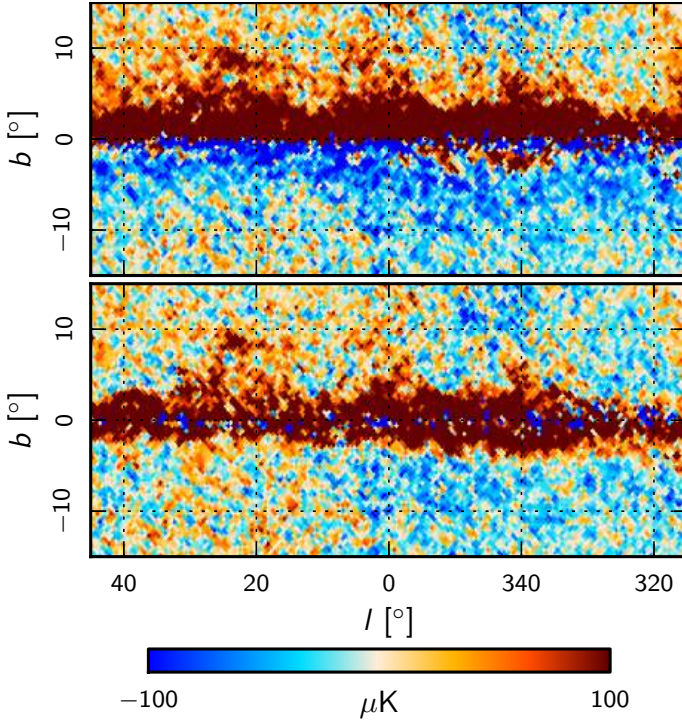
### 2.2.2. Survey difference method 2

The second method looks at one-dimensional slices through the Galactic Plane for each survey independently. The slices are taken along the scan direction and are constructed by averaging the sky signal over  $5^\circ$  in longitude. For this method, only the

sky region close to the Galactic Plane is considered (the region covers ten degrees above and below the Galactic Plane and longitudes between  $-40^\circ$  and  $60^\circ$ ). The Fourier Transform of the slice signal is convolved by the bolometer transfer function used to deconvolve the TOI and then deconvolved by the LFER4 transfer function with trial parameter values. New sky surveys are then obtained by re-projecting the slices into pixelized maps. As for the previous method, parameters of the low-frequency part of LFER4 transfer functions are chosen so that they minimize the residuals in the difference maps.

In practice, the first method is used for the 100–353 GHz bolometers, while at 545 GHz and 857 GHz the second method is better adapted to the maps having the most structure in the Galactic difference residuals. Figure 3 shows an example of the





**Fig. 3.** The Survey 2 minus Survey 1 residual close to the Galactic center before (upper) and after (lower) fitting and deconvolving the low frequency part of the time response for bolometer 353-2.

residual remaining in a *HEALPix*<sup>2</sup> map (Górski et al. 2005) of the survey difference after fitting the long time response, showing reduced asymmetry in the Galactic plane.

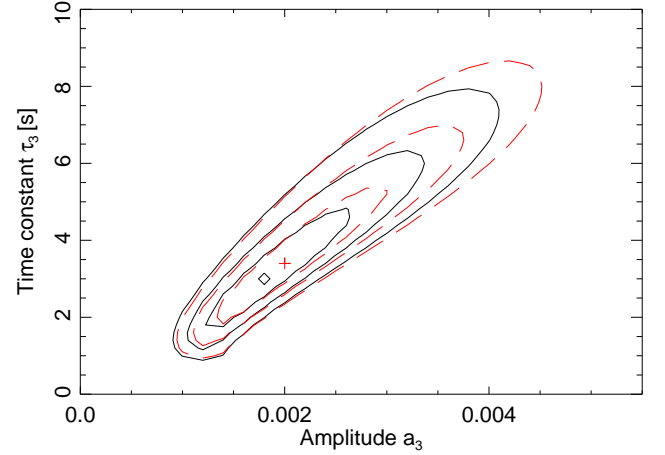
### 2.2.3. Survey difference systematics

In the survey difference solution for the time response, any systematic effect that creates a residual in the survey difference can be confused with a time response effect, in particular affecting the low frequency range of the time response. This section identifies a number of residual-producing systematics and quantifies the resulting bias in the transfer function. These residual-producing systematics include far sidelobes, zodiacal light, pointing offset uncertainty, gain drifts, main beam asymmetry and polarized sky signal.

Due to the very high signal to noise ratio of Galactic signal in the sub-millimeter domain, far sidelobe pickup of the Galactic plane is detected in the 545 GHz and 857 GHz channels. A physical optics model of the far sidelobe pickup is used to estimate the signal from the Galactic center. The optical depth of the zodiacal dust cloud along the line of sight varies as *Planck* orbits the Sun leaving a residual in the survey difference (Planck Collaboration XIV 2013). A model of the zodiacal dust emission is subtracted in the reconstruction of the time response. The reconstruction of the time response is then repeated without subtracting the models; it is found that these do not significantly affect the result (Fig. 4).

As a probe of the effect of far sidelobes on the time constant determination, the pipeline is run on a survey difference map obtained from the sidelobe model alone for each of the 100, 143, 217, and 353 GHz channels. The method did not find any long

time constant, as the sidelobe effect on the survey map is very different from the time constant effect.



**Fig. 4.** 68 %, 95 %, and 99 % likelihood contours for the long time constant  $\tau_3$  and associated amplitude  $a_3$  for a 545 GHz bolometer (545-4) with (black) and without (red) zodiacal emission and FSL removal. The square and cross indicate the maximum likelihood values.

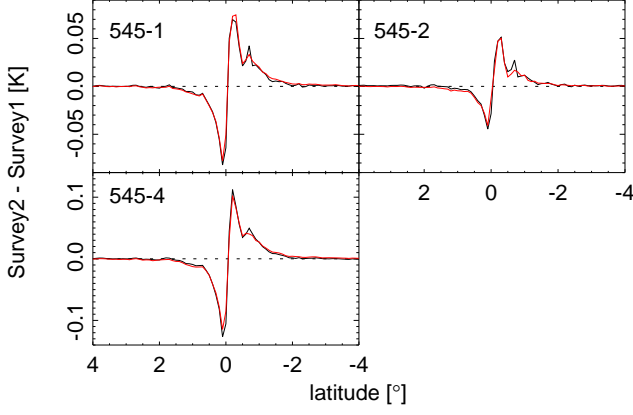
A systematic offset in the pixel pointing creates a residual in the survey difference. The pointing solution reduces the pointing error to a few arcseconds RMS in both the co-scan and cross-scan direction. With the  $6^\circ \text{s}^{-1}$  scanning speed, this error corresponds to frequencies greater than 1 kHz, far from the range affected by the long time constant.

Gain variability can also bias the estimation; due to nonlinearity in the analog to digital converters (ADC), HFI's responsivity to sky signal varies at a few tenths of a percent throughout the mission. As a probe of this effect, gain corrected data for the 100, 143 and 217 GHz bolometers are used to reconstruct the long time response. This is found to have a negligible impact on the fitted parameters. Residual gain errors tend to leave monopolar residuals that are not coupled to the long time constants in the fitting procedure.

Some residual is expected in the survey difference maps because the asymmetric beam scans the sky at different angles in the two surveys. This is especially an issue at 545 GHz where the beam is substantially asymmetric. To quantify the amplitude, simulated survey difference maps are generated using a realistic asymmetric beam model convolved with the Planck Sky Model; the residuals in the Galactic plane at 545 GHz are dominated by the main beam asymmetry (see Fig. 5).

Polarization Sensitive Bolometers (PSBs) show an additional residual in the survey difference maps because of polarized sky signal observed at slightly different crossing angles in the two surveys. For the PSBs, the low frequency time response is therefore determined using different levels of polarization masking. These studies do not suggest the presence of any significant level of bias from polarization, but only higher noise with wider masking. As an additional check on the contribution of residual polarization to the low frequency response, the survey difference of the sum of the a- and b- arms of each PSB pair is input to the pipeline. This sum is not sensitive to polarization, and no bias is found in the determination of the time response.

<sup>2</sup> <http://healpix.sf.net>



**Fig. 5.** Survey 1 minus survey 2 residual for the 545 GHz bolometers, averaged from Galactic longitude 0 through 20°. The black curves show the *Planck* data, and red is a simulation.

### 2.3. Fitting fast time constants with planet crossings

Filtering of the TOIs and errors in the deconvolution kernel results in ringing along the scan direction. The planets Mars, Jupiter and Saturn are high signal to noise sources that can be used to minimize this smearing by adjusting the parameters of the LFER4 model. See Sect. 3.1 for a description of the planet data.

In solving for the high frequency portion of the time response, the beam profile is forced to be compact. The optical beam is modeled as a spline function on a two-dimensional grid (see Appendix C for details) and the LFER4 parameters are fit by forcing conditions on the resulting beam shape (Fig. 6).

The planet data are first deconvolved with a time response model derived from pre-launch data to recover an initial estimate of the beam profile. Jupiter is used for the 100, 143 and 217 GHz channels while Saturn is used for higher frequencies (See Sect. 3.4 for a discussion of the nonlinearity of Jupiter at higher frequencies).

Rather than deconvolve the planet data, the model parameters are determined in the forward sense. Since the beam is decomposed into B-spline functions, this basis is convolved by the temporal transfer function to retrieve the coefficients for each basis function using the planet data. These coefficients are applied to the original deconvolved B-spline functions to recover an estimate of the optical beam. The convolution is made in the Fourier domain by re-sampling the B-spline function onto a timeline with a sample separation corresponding to 4''5. The typical knot separation length of the basis function is between 1' and 2'.

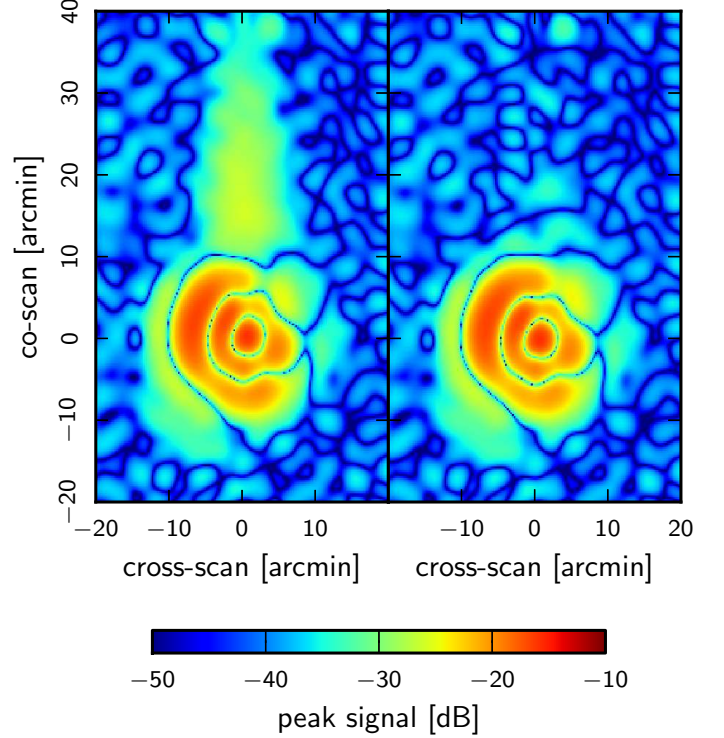
In the Fourier domain, the convolution of the temporal transfer function with the planet signal is

$$\mathcal{PC}(\omega) = \mathcal{B}^0(\omega) * \text{TF}^0(\omega), \quad (5)$$

where  $\mathcal{B}^0(\omega)$  is the Fourier transform of the slice through the peak planet signal in the scan direction  $b^0(t)$ , which is obtained by de-convolving planet data using a fiducial estimate,  $\text{TF}^0(\omega)$  of the transfer function. The cut  $b^0(t)$  is then symmetrized about the origin to obtain  $b^{\text{sym}}(t)$ , and its Fourier transform  $\mathcal{B}^{\text{sym}}(\omega)$ . This operation aims at recovering a beam that, by construction, is symmetric within the limits allowed by the model of the temporal transfer function,

$$\mathcal{PC}(\omega) = \mathcal{B}^{\text{sym}}(\omega) * \text{TF}^*(\omega). \quad (6)$$

Here  $\mathcal{B}^{\text{sym}}(\omega)$  is entirely defined by  $\mathcal{PC}(\omega)$  and  $\text{TF}^0(\omega)$  and the new estimate of the time response ( $\text{TF}^*(\omega)$ ) is derived from equation 6. This function is parameterized in terms of the three shortest time constants ( $\tau_1, \tau_2, \tau_3$ ) and their associated amplitudes ( $a_1, a_2, a_3$ ).



**Fig. 6.** Gridded Jupiter data for bolometer 143-3b before and after fitting for LFER4 parameters. The best fit Gaussian is subtracted from each plot to emphasize residuals. Residuals in the main beam show the deviation of the optical beam from a Gaussian shape, captured in the representations of the scanning beam as described in Appendices B and C.

### 2.4. Stationarity of the Time Response

The time response of each HFI detector/readout channel is a function of the cryogenic temperature of the bolometers and the ambient-temperature components of the readout electronics. Both cryogenic and ambient temperatures change throughout the mission as the Galactic particle flux and the *Planck* spacecraft solar distance are modulated. The seasonal consistency of the scanning beam sets an upper limit on changes in the time response through the mission, shown below in Section 5.2.1.

### 2.5. Deconvolution of the data

The time response transfer function is deconvolved from the data and not included as part of the scanning beam because the low frequency response of the bolometer would give an extended scanning beam stretching many degrees from the main lobe along the scan direction.

Since the time response amplitude decreases as a function of frequency, the deconvolution operation increases the noise at high frequency to an unacceptably high fraction of the RMS. During the deconvolution stage of the TOI processing, a phase-

less low-pass filter is applied in order to suppress the high frequency noise and keep pixel aliasing at a manageable level.

In the early data release, a finite impulse response low-pass filter was used for this purpose (Planck HFI Core Team 2011b). In the 2013 cosmology data release, the low-pass filter is further tuned for the 100, 143, 217 and 353 GHz channels to reduce filter ripple produced by the lowpass filters used in the early-release data. The filter is now implemented in the Fourier domain, with a kernel consisting of the product of a Gaussian and a squared cosine,

$$K(f) = K_1(f)K_2(f), \quad (7)$$

where

$$K_1(f) = \exp(-0.5(f/f_{\text{Gauss}})^2) \quad (8)$$

and

$$K_2(f) = \begin{cases} 1 & \text{if } f < f_c, \\ \cos^2\left(\frac{f-f_c}{f_{\text{max}}-f_c}\right) & \text{if } f_c < f < f_{\text{max}}, \\ 0 & \text{if } f > f_{\text{max}}. \end{cases} \quad (9)$$

$f_{\text{max}} = f_c + k(f_{\text{samp}}/2 - f_c)$  and  $f_{\text{samp}}$  is the sampling frequency of the data. The parameters of the filter are the same for all bolometers in the bands 100–353 GHz;  $f_{\text{Gauss}} = 65$  Hz;  $f_c = 80$  Hz, and  $k = 0.9$ . To first order, this filter widens the scanning beam along the scan in an equivalent way to convolving the optical beam with a Gaussian with Full-width at Half-maximum (FWHM) 2'.07. The filter introduces some rippling along the scan direction at the  $-40$  dB level at 217 and 353 GHz where the beams allow harmonic signal content close to the filter edge. The rippling is captured by the B-spline beam representation (see Fig. 11).

The 3-point finite impulse response filter is still used for the 545 and 857 GHz channels<sup>3</sup>. This extends the scanning beams along the scan direction more than the Gaussian-cosine Fourier filter (the 545/857 GHz filter time scale corresponds to 3'.0 on the sky), but has the advantage of reducing rippling and signal aliased from above the Nyquist frequency.

The deconvolution kernel multiplied by the data in the Fourier domain is the product of the lowpass filter with the inverse of the bolometer/electronics time response,

$$D(f) = K(f)/\text{TF}(f). \quad (10)$$

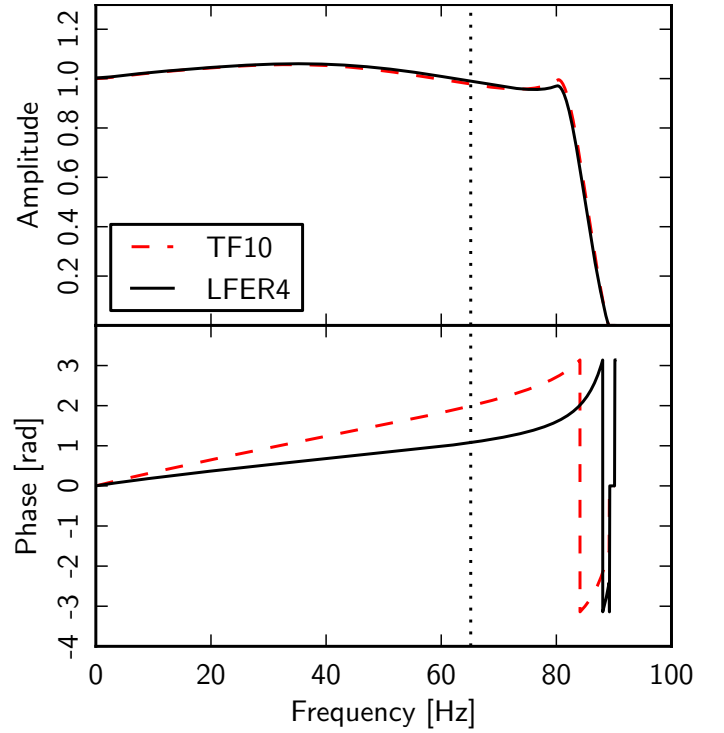
See Fig. 7 for a comparison of the deconvolution functions resulting from the LFER4 model and from the TF10 model used in the ERCSC data. The differences between the two models appear mainly in the phase at high frequency, mostly above the signal frequency corresponding to the beam size. Although the phase of LFER4 is a more accurate description of the system, in practice replacing LFER4 with TF10 had little effect on the data because of the lowpass filter applied at the time of deconvolution and the empirical determination of an overall sample offset in the pointing reconstruction.

In the HFI data processing (Planck Collaboration VI 2013), data chunks of length  $2^{19} \approx 5 \times 10^5$  samples are Fourier transformed at a time, overlapping by half with the subsequent chunk to avoid edge effects.

### 3. Scanning Beams

Filtering of the TOI and the accuracy of the deconvolution kernel affect the angular response of the HFI detectors. An accurate estimate of the *scanning beam*, resulting from the filtering of the

<sup>3</sup> The data are convolved with the kernel [0.25, 0.5, 0.25] in the time domain.



**Fig. 7.** The phase and amplitude as a function of signal frequency of the deconvolution function of bolometer 217-1. The solid black curve is the LFER4 model, while the dashed red curve shows the TF10 model used in the Early Papers. The vertical dotted line marks the signal frequency corresponding to the half power point of the average effective beam.

physical (optical) beam by these time domain convolutions, is required to relate the angular power spectra of the maps to that of the underlying sky. As described in Planck HFI Core Team (2011a) and Planck HFI Core Team (2011b), HFI's scanning beam profiles are measured using the planetary observations. The HFI uses two flat sky representations of the two-dimensional scanning beam: one using Gauss-Hermite polynomials and another using B-spline functions.

Three selections of planetary data are used to derive estimates of different aspects of the beam:

1. The first two observing seasons of Mars (main beam, and window functions).
2. All available seasons of Mars [3], Jupiter [5] and Saturn [4] (near sidelobe).
3. All five Jupiter observations (residual time response).

The effective beam window functions used in the CMB analysis are ultimately derived from the first of these. In each case, the statistical properties of the beam representations and the choice of planetary data are studied using ensembles of simulated planet observations (Section 5).

While the signal to noise ratio of the Jupiter and Saturn data is significantly greater than the Mars data, at this stage of the analysis a reconstruction bias results in the main beams recovered from *simulated* Jupiter and Saturn observations that is *not* present in the simulations of Mars. Additionally, the nonlinear response of some HFI detectors to the Jupiter signal (Planck HFI Core Team 2011a) makes the normalization of the planet peak response uncertain at the few percent level (see Sect. 3.4). Therefore the main beam model is established using Mars data,



**Table 1.** Observation seasons of the planets observed by *Planck*: date range and position in Galactic coordinates.

Planet	Season	Date Range	$l$ [°]	$b$ [°]
Mars	1	22/10/09–29/10/09	204.3	30.6
	2	10/04/10–15/04/10	203.3	31.5
	3	20/12/11–25/12/11	251.3	60.5
Jupiter	1	25/10/09–29/10/09	33.6	−40.2
	2	03/07/10–09/07/10	102.4	−61.4
	3	06/12/10–12/12/10	83.8	−61.0
	4	03/08/11–09/08/11	156.4	−43.0
	5	10/01/12–13/01/12	147.5	−49.2
Saturn	1	04/01/10–08/01/10	286.0	62.2
	2	11/06/10–17/06/10	271.6	62.5
	3	18/01/11–22/01/11	310.3	58.2
	4	29/06/11–05/07/11	298.4	60.9
Uranus	1	05/12/09–10/12/09	81.3	−60.1
	2	30/06/10–05/07/10	97.3	−60.9
	3	10/12/10–15/12/10	89.2	−60.8
	4	05/07/11–10/07/11	105.4	−60.6
	5	22/12/11–26/12/11	97.4	−60.9
Neptune	1	31/10/09–05/11/09	39.9	−44.5
	2	17/05/10–22/05/10	45.0	−48.1
	3	03/11/10–07/11/10	42.0	−46.1
	4	20/05/11–25/05/11	47.4	−49.6
	5	16/11/11–20/11/11	44.3	−47.7

while observations of Jupiter and Saturn are used only to estimate the near sidelobes and residuals in the deconvolution of the transfer function.

The B-spline representation of the joint Mars observations is used as input for the calculation of the effective beam and the effective beam window function. Simulations have shown the B-spline representation to better capture the features outside of the main lobe, due to the necessarily finite order of the Gauss-Hermite decomposition. The Gauss-Hermite model is used for other systematics checks, including the consistency of the planets and observing seasons.

Because the Jupiter and Saturn data allow measurement of the beam response below −45 dB from the peak, there is no need to rely on a model of the telescope to determine the main beam or near sidelobe structure.

### 3.1. Planetary Data Handling

The JPL Horizons package<sup>4</sup> (Giorgini et al. 1996) is programmed with *Planck*’s orbit to calculate the positions of the planets. Table 1 shows the dates when the planets were within 2° of the center of the focal plane. By the end of HFI’s mission Mars was observed three times, Saturn four times and Jupiter five.

The planets Jupiter, Saturn and Mars are among the brightest compact objects seen by *Planck* HFI; the signal amplitude affects the data handling in a number of ways. Moving solar system objects are flagged and removed from the TOI in the standard processing pipeline. A specialized processing for the planet data is required, with two major differences from the nominal processing (see Planck Collaboration VI (2013) for details).

While the pickup from the <sup>4</sup>He-JT cooler is removed from the data as usual, pointing periods containing very bright sources

such as the planets cannot be used to reliably estimate the line amplitude. Instead, during the planet observations, these are extrapolated from neighboring pointing periods.

To better detect glitches near the extremely bright planet crossings, an estimate of the planet signal is subtracted from the data prior to glitch detection. Glitch template subtraction is performed on the signal subtracted timeline in the same way as during nominal observations.

In order to remove the (quasi-stationary) astrophysical background from the planetary data time lines, a bilinear interpolant of the frequency averaged map is subtracted from the data. The full mission map is used for the five-season Jupiter data, while the nominal survey sky maps are used in the processing of the other planetary data.

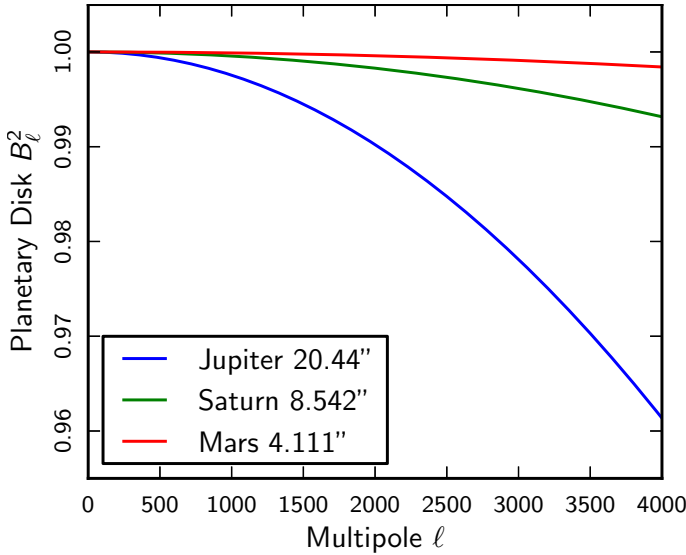
The planets are oblate spheroids, and appear as ellipses slightly extended along the direction of the ecliptic. The *Planck* planet range and *Planck* sub-latitude calculated by JPL Horizons are used in combination with the polar and equatorial radii of the planets reported by Horizons to compute the angular size and ellipticity of each planet. During HFI’s observations, the mean angular radii of Jupiter, Saturn and Mars are 20′44, 8′542, and 4′111, respectively. The ratio of the equatorial to polar radii are 1.069, 1.109 and 1.006, respectively.

The finite planetary disk size increases the apparent size of the scanning beam and biases the inferred effective beam window function. The filtering in multipole space of a circular disk of angular radius  $R$  can be written as  $B_{\text{disk}}(\ell) = 2J_1(\ell R)/(\ell R)$ , where  $J_1(x)$  is the Bessel function of order 1. Figure 8 shows the  $B_{\text{disk}}^2(\ell)$  for the three planetary disks. In practice, the effects of the disk size are mitigated by merging observations from the three brightest planets. The effects of the large Jupiter disk size are greatest where the spatial gradient of the beam is greatest, between the −3 to −10 dB contours of the beam. By excluding the Jupiter observations above −10 dB, the disk size smearing is reduced, and setting a −20 dB threshold results in a bias in the window function below  $10^{-3}$  at all multipoles.

*Planck* observes Saturn at a range of ring inclination angles: 6°03, 2°45, 12°6 and 9°4 for seasons 1, 2, 3 and 4, respectively. While emission from the solid angle of the ring increases the effective planetary disk area, the brightness temperature of the ring tends to be much less than the planetary disk temperature for the *Planck* bands. For example Weiland et al. (2011) fit a single 90 GHz ring brightness temperature that is 14 % that of the Saturn disk. In our beam reconstruction the average of the first three *Planck* observations of Saturn is used, and even in the extreme limit where the ring brightness temperature is the same and only Saturn data are used, the multipole space correction is  $2 \times 10^{-3}$  at  $\ell = 3000$ ; this correction is ignored.

The elliptical shape of the planetary disk gives a further bias in the inferred window function, depending on whether the long axis of the beam is aligned with or perpendicular to the long axis of the planet. In this case the planetary disk is approximated as an elliptical Gaussian with  $\sigma = 0.5R$ . The worst case is a  $10^{-3}$  effect in the case of 100 GHz beams measured on Jupiter at  $\ell = 3000$  (where the 100 GHz window function is vanishingly small). At 143 and 217 GHz, the  $10^{-3}$  level is reached only at  $\ell = 4000$ . The effect is negligible in the range of *Planck*’s sensitivity. With Saturn and Mars, the ellipticity effects are  $< 10^{-4}$  and  $< 10^{-6}$  respectively at all multipoles; the ellipticity of the planetary disks has a negligible effect on the estimate of the scanning beam.

<sup>4</sup> <http://ssd.jpl.nasa.gov/?horizons>



**Fig. 8.** Window functions of the planetary disks of Jupiter, Saturn, and Mars, equivalent to the bias in the inferred effective beam window function if the beam is reconstructed from observations of one of these planets alone. The labels show the corresponding angular radius of each disk.

### 3.2. Main Beam Model

Two representations are used to describe the (two dimensional) main beam; a Gauss-Hermite basis (described in Appendix B following Huffenberger et al. (2010) and Planck HFI Core Team (2011a)) and a B-spline basis (Appendix C).

The Gauss-Hermite (GH) and B-spline bases have very different characteristics. The GH representation uses a relatively small number of parameters and, in practice, amounts to a perturbative expansion about a Gaussian shape. The B-spline is quite general, using many more degrees of freedom to fit the data on a defined grid with the spline controlling the behaviour in between. The bias and correlation structure of the noise of these two representations are characterized using Monte Carlo simulations of the planetary data that include all the details of the beam processing pipeline used on the data (These simulations are described more completely in Section 5). In each case, the parameters of the representation are derived directly from the time-ordered data, without recourse to a pixelized map.

Figure 9 shows the B-spline scanning beams for the entire HFI focal plane as reconstructed from the Jupiter and Saturn data. Figure 10 shows the radially binned, frequency averaged beam profile for the HFI channels, comparing the B-spline representation of the Mars data (solid black lines) with the combined Mars, Jupiter and Saturn data (filled and open points, and the blue dashed line). The B-spline maps are apodized with a Gaussian at a radius beyond the signal to noise floor of the Mars data.

The azimuthally averaged beam window function,  $B_\ell^2$ , from each of these models is compared to the known input beam model. At 100, 143 and 217 GHz the two methods perform comparably, with the B-spline having slightly smaller bias and variance; at the higher frequencies the B-spline performs demonstrably better, especially at 545 and 857 GHz, as expected due to the highly non-Gaussian shape of these multi-mode detectors.

### 3.3. Near Sidelobes

While the HFI's beams are highly Gaussian at the  $-25$  dB level, non-trivial structure in the beam is captured in the data at lower power. There are two distinct components to the near lobe response; a discrete pattern of secondary lobes evident at frequencies of 217 GHz and above, and a diffuse shoulder consistent with phase errors in the aperture plane.

The Planck reflectors suffer from print-through of the honeycomb structure that supports the carbon-fiber face sheets. The size of the deformation has been measured during thermal testing to be less than  $20\mu\text{m}$  (Tauber et al. 2010). While small in amplitude, the strict periodicity of this pattern results in a correspondingly periodic structure in the near lobes, seen clearly in Fig. 12, that is slightly larger than predicted based on the pre-launch measurements. A simple grating equation describes the angular positions of the resulting contributions to the near sidelobes,

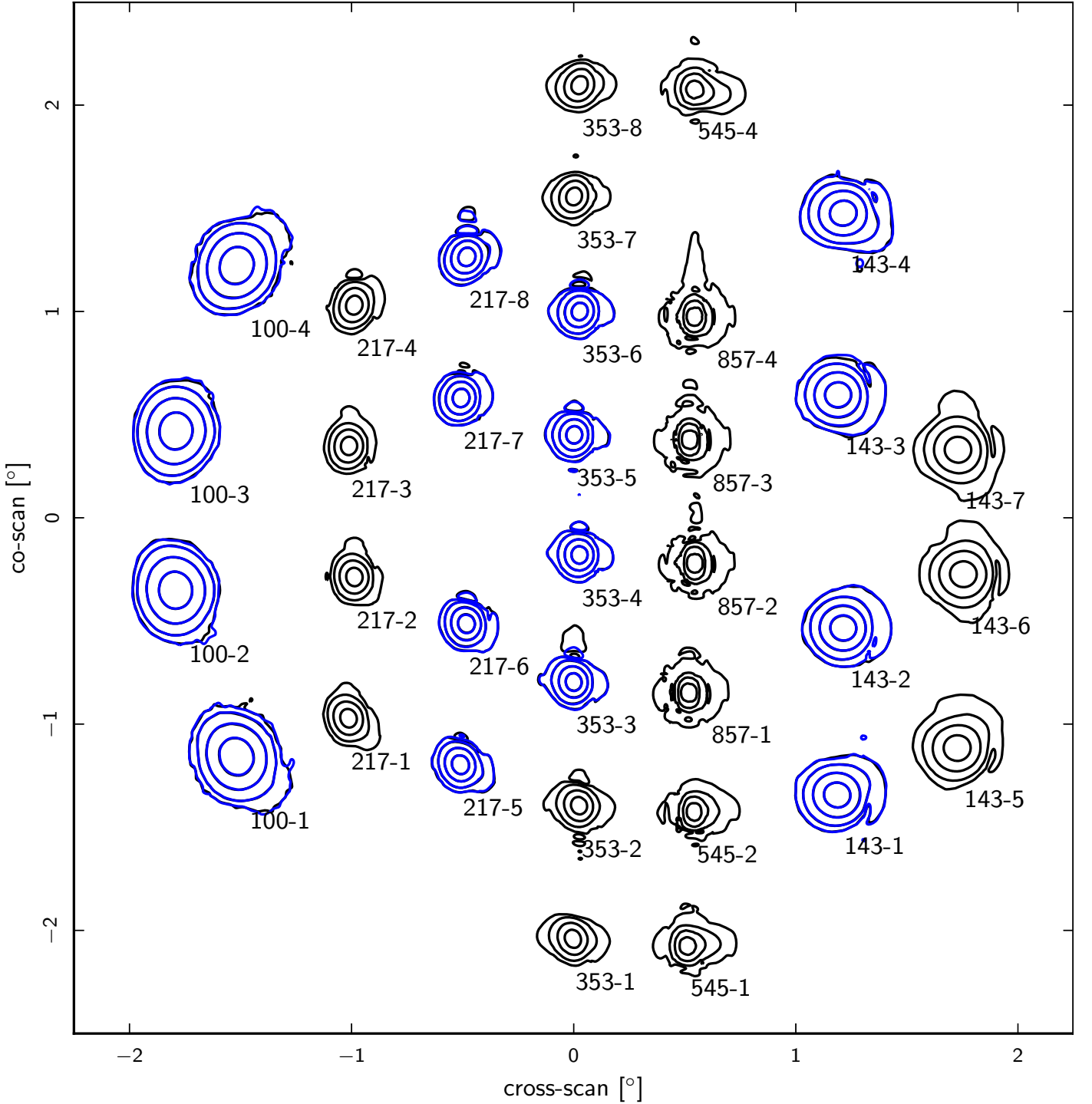
$$\sin \theta_n = \frac{n\lambda}{Yd}. \quad (11)$$

where  $\theta_n$  is the angular position of the  $n$ 'th order lobe from the central beam peak;  $\lambda$  is the wavelength of the radiation;  $d$  is the grating periodicity and  $Y$  is a factor that describes the position of each reflector along the optical path.  $Y = 1.00$  for the primary reflector and  $Y = 1.80$  for the secondary reflector. Three possible periodicities (19.6 mm, 30 mm, 52 mm) in the honeycomb array dominate the Planck dimpling pattern for the 857 GHz detectors, though only those for the 52 mm can be seen for the 545 GHz and 353 GHz detectors. For the highest frequency detectors, only the weaker lobes due to the 19.6 mm and 30 mm periodicities are seen outside the  $40'$  main beam model, but they contribute at most  $(0.05 \pm 0.008)\%$  to the integrated beam solid angle. A forthcoming publication (Oxborrow 2013) will present an in-depth study of the mirror surface.

The second component is a beam shoulder becoming significant near the  $-30$  dB contour, and extending to 2-4 FWHM from the beam center. This shoulder is consistent with scattering from random surface errors on the primary and secondary reflectors, and is reasonably well-described by a spectrum of surface errors with correlation lengths ranging from 2 to 12 cm with an RMS of order  $10\mu\text{m}$  (Ruze 1966). The contribution of each of these components is included in the radially binned profiles shown in Fig. 10.

While the B-spline parameterization captures both the main beam and near sidelobe structure, the extended features must be separately included in the Gauss-Hermite beam representation. See Fig. 11 for a contour plots of a B-spline beam using Mars, Jupiter and Saturn data at each frequency.

The B-spline representation of the scanning beam that is used to compute the window function includes only that portion of the near sidelobe structure that falls within the signal to noise of the Mars data; the Jupiter and Saturn data provide an estimate of the beam solid angle that is neglected in the scanning beam product. The near sidelobe solid angle, and the resulting window function error, are sensitive to the details of the analysis, including the sky subtraction, offset removal and masking of in-scan ringing at the part-per-million level. Although a comprehensive study of these effects in the Jupiter and Saturn data are underway a conservative, and model independent upper limit is obtained by taking the envelope of the noise floor to define the maximum solid angle allowed by the data (the red dashed line in Fig. 10). A reasonable estimate of the true solid angle in the near lobes can be obtained by extrapolating the data below the noise floor (the blue dashed line in Fig. 10). By either measure, the grat-



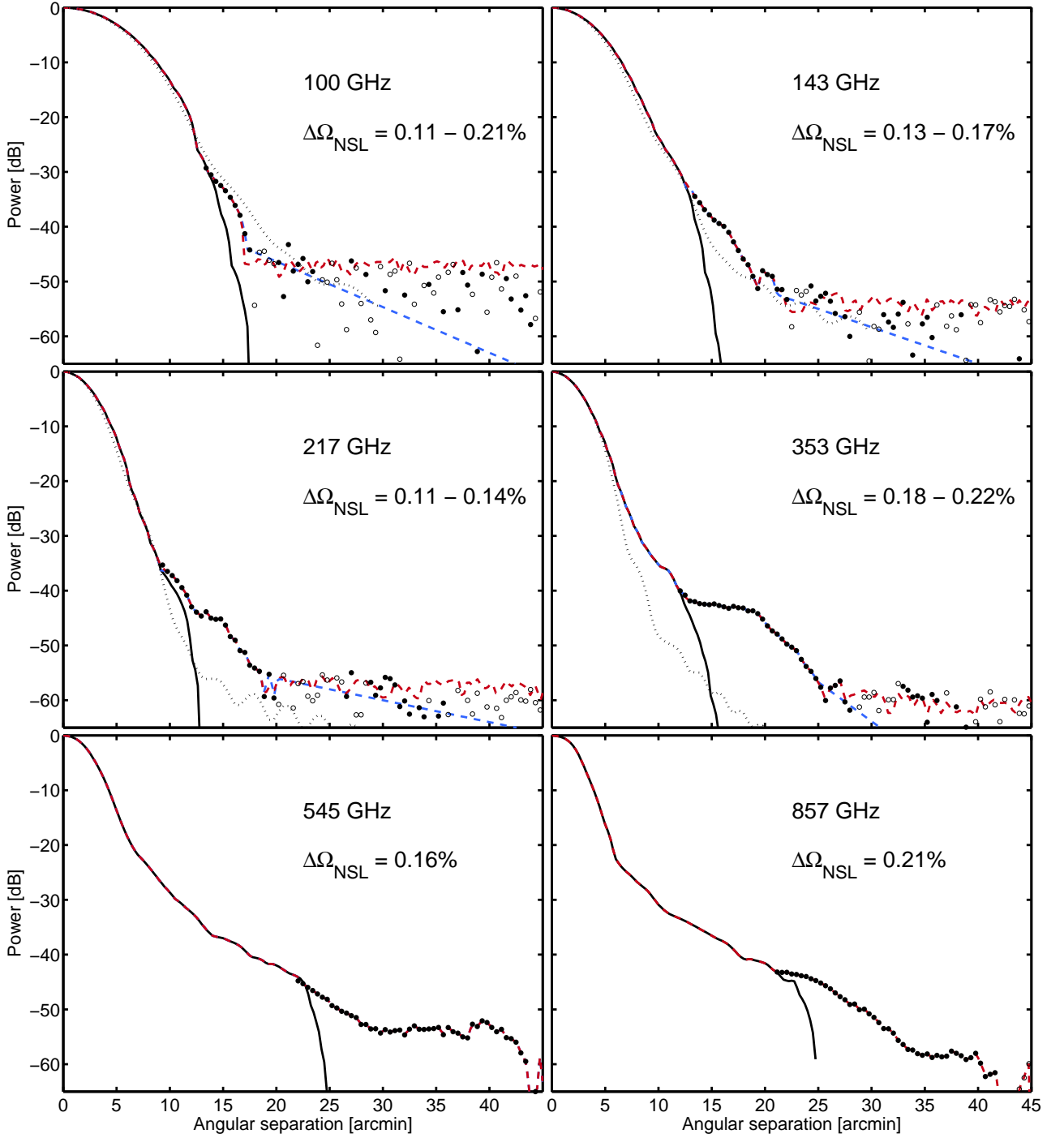
**Fig. 9.** B-spline scanning beam profiles reconstructed from Mars, Saturn, and Jupiter seasons 1, 2 and 3 data for near sidelobe studies. The beams are plotted in logarithmic contours of  $-3$ ,  $-10$ ,  $-20$  and  $-30$  dB from the peak. PSB pairs are indicated with the  $a$  bolometer in black and the  $b$  bolometer in blue.

ing lobes and diffuse shoulder account for a small fraction of the total beam solid angle; for the 100, 143 and 217 GHz channels this contribution represents less than 0.15 % of the total solid angle (see Table 2). The amplitude of the impact on the window function is estimated by comparing the Legendre transform of the maximal envelope of the Jupiter and Saturn data with that of the nominal Mars derived scanning beam. The result is shown as the family of green curves in Fig. 19. Because the Monte Carlo ensembles that are used to derive the error envelope neglect this near sidelobe structure in the beam that is input to the simula-

tions, the window function error amplitudes have been scaled to accommodate the upper limit defined by the noise floor of the Jupiter and Saturn data.

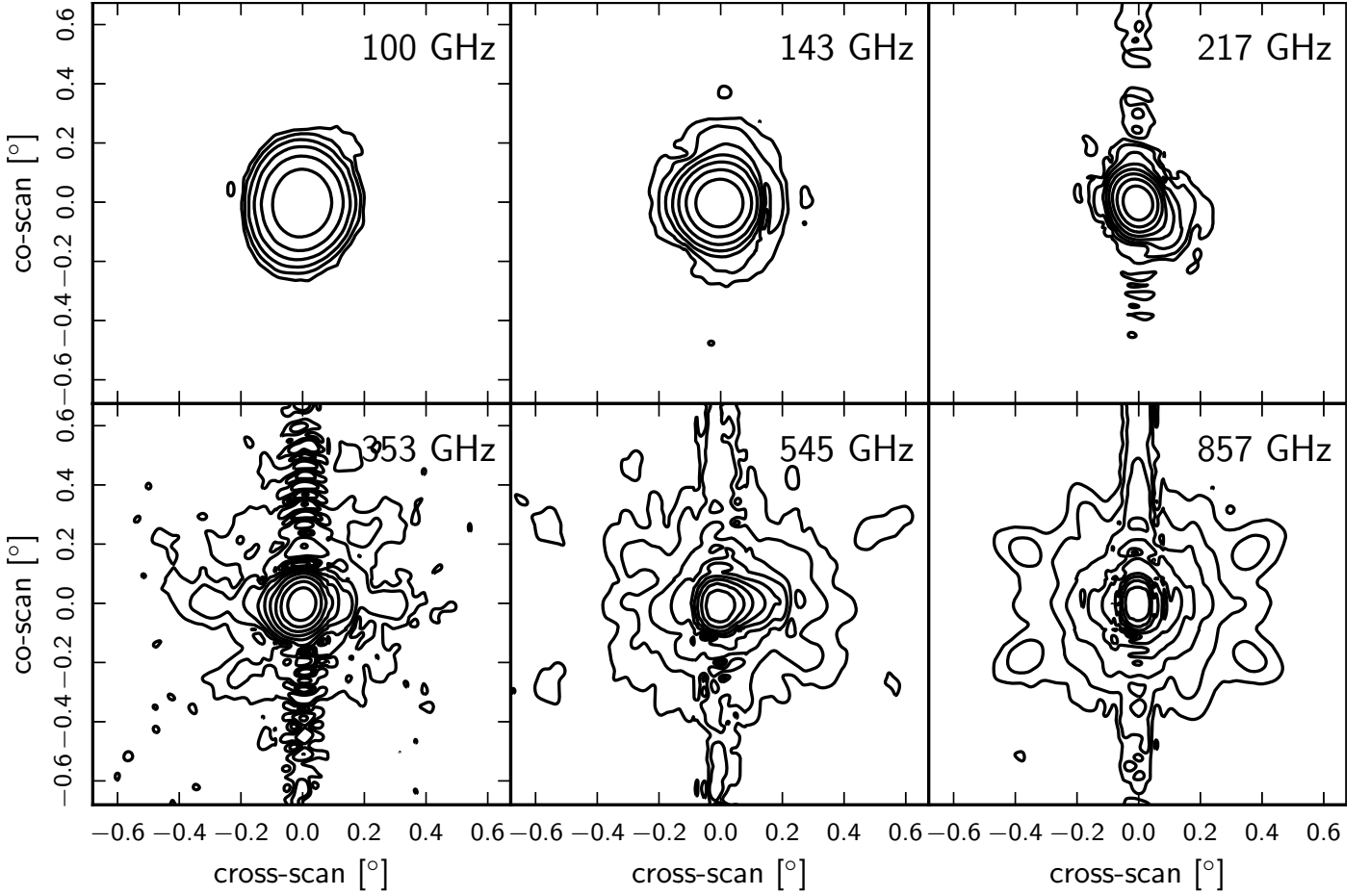
### 3.4. Residual Time Response

The *Planck* spacecraft spin rate is constant to 0.1 %, making the time response of the electronics and the bolometer degenerate with the angular response of the optical system.



**Fig. 10.** The azimuthally and band averaged main beam profiles (black solid curve) derived from the B-spline representation of the first and second Mars observations compared to that derived from a combination of Mars, Jupiter and Saturn observations (filled and open markers represent positive and negative data respectively). The red dashed line is defined as the joint envelope of the main beam and near sidelobe dataset, the integral of which represents the maximal solid angle that is compatible with these data. A nominal near lobe model, provided as a reasonable extrapolation of the data below the noise floor, is shown as the blue dashed line. The fractional increase in solid angle, relative to the Mars-alone derived beam profile, is displayed in each panel. The black dotted line shows the GRASP physical optics model averaged over a subset of detectors that have been simulated (100–353 GHz). The data show a clear excess in power over the model at 143, 217 and 353 GHz that is consistent with a spectrum of surface errors on scales between 2 and 12 cm, with an RMS of order  $10\mu\text{m}$ . Table 2 contains an estimate of the fraction of the solid angle in the near sidelobes that is not captured in the B-spline representation. For clarity, the figure extends only to  $45'$ . In all cases the solid angle is derived from the profile extending out to five degrees. Due to the high signal to noise of the Jupiter data ( $-40$  to  $-55$  dB, depending on the frequency), and the rapidly falling response of the beam, the solid angle estimates are insensitive to the limit of integration.





**Fig. 11.** One scanning beam at each HFI frequency (100-3b, 143-6, 217-1, 353-7, 545-1, and 857-3). Contours are in dB from the peak in steps of  $-5$  dB. The lowest contours are set at  $-30$  dB,  $-35$  dB,  $-40$  dB,  $-45$  dB,  $-45$  dB,  $-45$  dB at 100 GHz, 143 GHz, 217 GHz, 353 GHz, 545 GHz, and 857 GHz respectively.

The B-spline beam model extends  $\pm 20'$  from the center of the beam. An error in the time response on fast time scales will thus be exactly compensated by the scanning beam. However, errors in the time response beyond the limit of the scanning beam reconstruction will not be accounted for and will tend to bias the recovered beam window function.

To look for residual long tails due to incomplete deconvolution of the time response, all five seasons of Jupiter observations are binned into a 2D grid of  $2'$  pixel size extending  $6^\circ$  from the planet (Fig. 12). These are background-subtracted using the *Planck* maps and stacked by fitting a Gaussian to estimate the peak amplitude and centroid of each observation. The data are binned as a function of pointing relative to the planet center.

While a static nonlinearity correction is included in the TOI processing, partial ADC saturation and dynamical nonlinearity bias the normalization of these tails by underestimating the Jupiter peak signal. An estimate of the nonlinear correction is derived by fitting a gridded map of all three Mars observations to a map of all five Jupiter observations for each detector. A signal reduction at the peak of Jupiter is ruled out at 1 % level at 100 and 143 GHz, but detected at higher frequency. Relative to Mars, the peak Jupiter signal is reduced by nonlinearity on average by  $3 \pm 3$  %,  $12 \pm 3$  %,  $12 \pm 4$  % and  $65 \pm 20$  % at 217, 353, 545 and 857 GHz respectively. The tail normalizations are scaled by these factors.

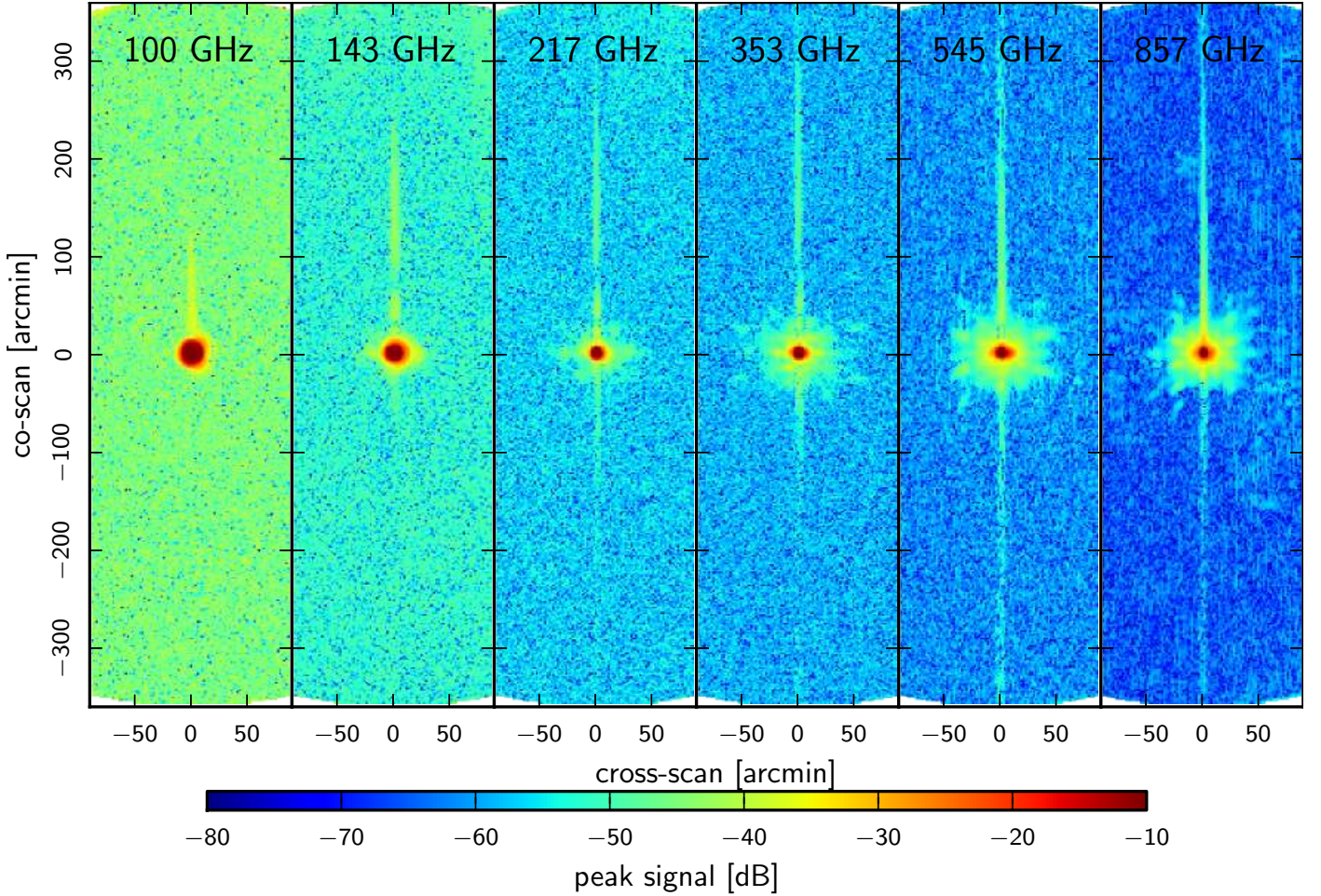
An example of the residual tail is shown in Fig. 13. As well as a tail following the planet due to imperfect deconvolution of

the time response, there also is a tail preceding the planet crossing; this is due to the lowpass filter applied in the Fourier domain. The residual beam tails have amplitudes typically at the level of  $10^{-4}$  of the peak but extend several degrees from the center of the beam. The response beyond  $6^\circ$  on the sky is consistent with noise for all detectors.

These stacked Jupiter data are integrated to determine the expected bias in total beam solid angle from this remaining uncorrected time response (see Table 2). The mean integral values are typically at a few times  $10^{-4}$  of the main beam solid angle, an order of magnitude lower than the error in the beam solid angle due to noise and other systematics.

The residual scanning beam tails can also bias the effective beam window function. The spherical harmonic transform of the residual that is not included in the model for the main scanning beam is computed,  $B_{\ell m}^{\text{full}} = B_{\ell m}^{\text{main}} + B_{\ell m}^{\text{tail}}$ , where  $B_{\ell m}^{\text{main}}$  is the multipole space representation of the main scanning beam model and  $B_{\ell m}^{\text{tail}}$  is the multipole space representation of the long tail model. In all cases, the  $m=0$  (symmetric) mode of the ratio of  $B_{\ell m}^{\text{full}}$  to  $B_{\ell m}^{\text{main}}$  dominates higher order modes by a factor of 1000, meaning that the coupling to the scan strategy is negligible and the bias in the effective beam window function can be approximated,

$$\delta W_\ell = \sum_m \frac{|B_{\ell m}^{\text{full}}|^2}{|B_{\ell m}^{\text{main}}|^2} - 1. \quad (12)$$



**Fig. 12.** Gridded data from all five seasons of Jupiter. The colour scale shows the absolute value of the peak signal.

The main effect on the effective beam window function is, at low  $\ell$ , the bias  $\delta W_\ell$  approaches a value of twice the fractional contribution to the total solid angle. When the window function is normalized to unity at the dipole frequency, the effect is a roughly constant bias in the window function at a level of a few  $\times 10^{-4}$  for  $\ell > 100$ . The contribution of the residual tail to the window function is neglected in the error budget.

### 3.5. Far Sidelobes

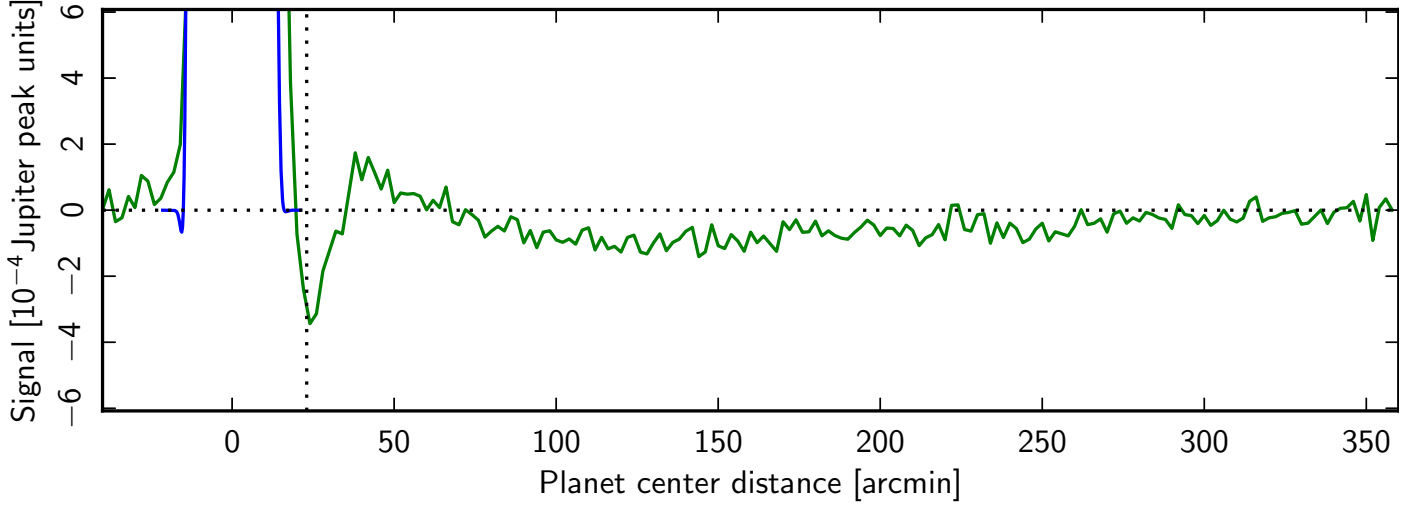
The far sidelobes (FSL) are defined as the response of the instrument at angles  $> 5^\circ$  from the main beam centroid. Tauber et al. (2010) describes the pre-launch measurements and predictions of the far sidelobe response using physical optics models. Figure 14 compares the measured beam profile of detector 353-1 with the FSL physical optics model. The way the FSL are treated in the dipole calibration and in the scanning beam model affects the effective beam window function, and care is needed to check whether the off-axis response could bias the window function at  $\ell > 40$  (angular scales  $< 5^\circ$ ) relative to  $\ell < 40$  (angular scales  $> 5^\circ$ ). To the extent that the physical optics simulations correctly predict the far sidelobe response (which is shown to be roughly the case in the survey difference maps), they produce effects negligible in the effective beam window function of HFI. Appendix D presents the details of this calculation.

Neglecting the far sidelobe effects depends on the quality of the physical optics model. Planck Collaboration XIV (2013) attempt a template fit of the physical optics model to the sur-

vey difference maps in combination with a zodiacal light model. While taking the survey difference removes roughly a factor of two of the sidelobe response, a substantial range of direct signal is removed. The template fits are presented in Table 4 of Planck Collaboration XIV (2013). The FSL signature is clearly detected at 857 GHz at a level much higher than predicted. As these channels are multi-moded, the differences are not that surprising; it is very difficult to do the calculations necessary for the prediction. In addition, the specifications for the horn fabrication were quite demanding, and small variations, though still within the mechanical tolerances, could give large variations in the amount of spillover.

For the lower frequency, single-moded channels, there is no clear detection of primary (PR) spillover (pickup from close to the spacecraft spin axis; see Appendix D). While the significant negative values may indicate some low-level, large-scale systematic, there seems to be nothing with the distinctive signature of primary spillover at frequencies between 100 and 353 GHz. These values indicate that the PR spillover values in Table 2 of Tauber et al. (2010) may be overestimated.

For the direct contribution of the secondary (SR) spillover, the situation is similar at 353 GHz, but at 217 and 143 GHz, there is a  $3\sigma$  detection at about the level expected, while at 100 GHz the value is about 2.5 times higher than expected, though the signal-to-noise on the detection is less than  $2\sigma$ . The baffle contribution to the secondary spillover appears higher than predicted, though Planck Collaboration XIV (2013) note that the

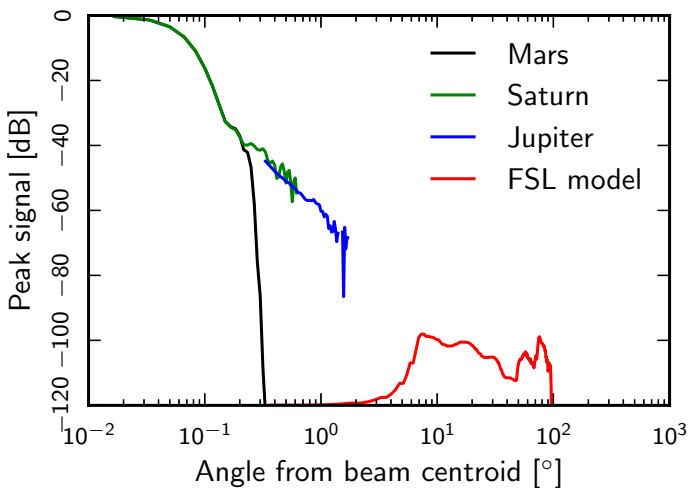


**Fig. 13.** A slice through stacked Jupiter data for bolometer 143-6 illustrating residual long time response after deconvolution. The vertical dotted line shows the extent of the scanning beam map (plotted in blue).

**Table 2.** Scanning beam solid angle ( $\Omega_{SB}$ ) error budget, showing the bias and fractional error due to the residual time response ( $\Delta\Omega_\tau$ ), near sidelobes ( $\Delta\Omega_{NSL}$ ) and solid angle colour correction ( $\Delta\Omega_{CC}$ ). The Monte Carlo error ( $\Delta\Omega_{MC}$ ) includes noise and pointing uncertainty. The colour correction is the upper limit in solid angle change due to colour correction from a planet spectrum source (roughly  $\nu^2$ ) to IRAS-convention ( $\nu^{-1}$ ). The near sidelobe contribution of the nominal (maximal) near sidelobe envelopes is shown for the 100 – 353 GHz bands; there is no appreciable difference between the two in the sub-mm bands, due to the extremely high signal to noise of these data.

Band [GHz]	$\Omega_{SB}$ [arcmin <sup>2</sup> ]	$\Delta\Omega_\tau$	$\Delta\Omega_{NSL}$	$\Delta\Omega_{CC}$	$\Delta\Omega_{MC}$
100	104.2	$-0.03 \pm 0.04 \%$	0.11 (0.21) %	$< 0.3 \%$	0.53 %
143	58.4	$-0.03 \pm 0.01 \%$	0.13 (0.17) %	$< 0.3 \%$	0.14 %
217	26.9	$-0.03 \pm 0.01 \%$	0.11 (0.13) %	$< 0.3 \%$	0.11 %
353	25.1	$-0.002 \pm 0.01 \%$	0.18 (0.22) %	$< 0.5 \%$	0.10 %
545	25.4	$0.04 \pm 0.01 \%$	0.16 %	$< 2.0 \%$	0.13 %
857	23.0	$0.09 \pm 0.01 \%$	0.21 %	$< 1.0 \%$	0.15 %

baffle spillover is difficult to model and the diffuse signal is easily contaminated by other residuals in the survey difference.



**Fig. 14.** Azimuthally averaged profiles of measured beams of channel 353-1 compared to the azimuthal average of the far side-lobe physical optics model.

#### 4. Effective Beams

Unlike *WMAP* (Jarosik et al. 2011), for large portions of the sky the scan strategy of *Planck* does not azimuthally symmetrize the effect of the beams on the CMB map. Treating the beams as azimuthally symmetric leads to a flawed power spectrum reconstruction. To remedy this, the effective beam takes into account the coupling between the azimuthal asymmetry of the beam and the uneven distribution of scanning angles across the sky.

The effective beam is computed at each HFI frequency scanning beam and scan history in real space using the FEBeCoP (Mitra et al. 2011) method as in *Planck*'s early release (Planck HFI Core Team 2011b). A companion paper describes the details of the application of FEBeCoP to *Planck* data (Rocha 2013).

FEBeCoP calculates the effective beam at a position in the sky by computing the real space average of the scanning beam over all crossings angles of that sky position. The observed temperature sky  $\tilde{\mathbf{T}}$  is a convolution of the true sky  $\mathbf{T}$  and the effective beam  $\mathcal{B}$ ,

$$\tilde{\mathbf{T}} = \Omega_{\text{pix}} \mathcal{B} \otimes \mathbf{T}, \quad (13)$$

where  $\Omega_{\text{pix}}$  is the solid angle of a pixel, and the effective beam can be written for the temperature in terms of the pointing matrix  $A_{ti}$  and the scanning beam  $P(\hat{r}_j, \hat{p}_t)$  as

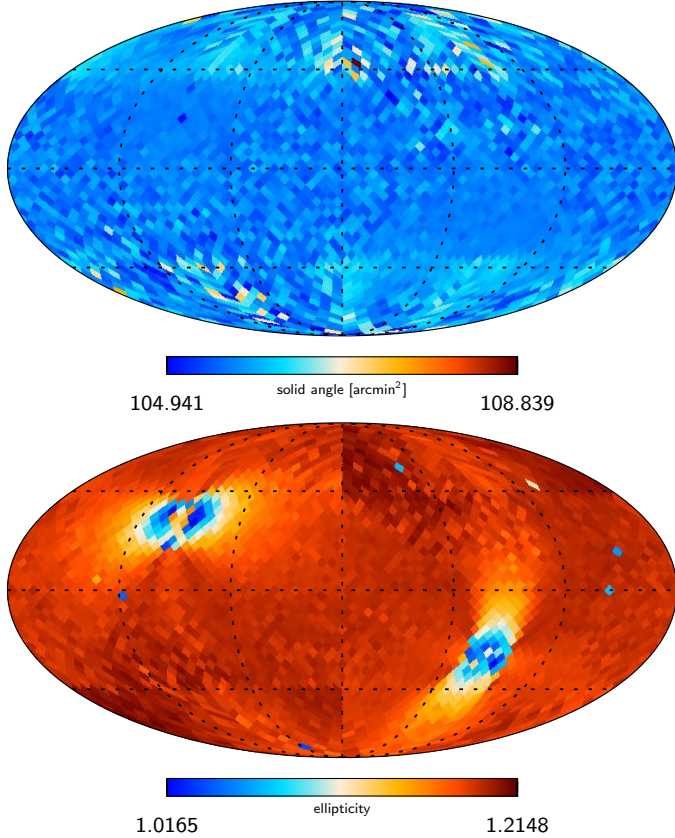
$$\mathcal{B}_{ij} = \frac{\sum_t A_{ti} b(\hat{r}_j, \hat{p}_t)}{\sum_t A_{ti}}, \quad (14)$$



$t$  is the time-ordered data sample index and  $i$  is the pixel index.  $A_{ti}$  is 1 if the pointing direction falls in pixel number  $i$ , else it is 0,  $\mathbf{p}_t$  represents the pointing direction of the time-ordered data sample, and  $\hat{\mathbf{r}}_j$  is the center of the pixel number  $j$ , where the scanning beam  $P(\hat{\mathbf{r}}_j, \mathbf{p}_t)$  is being evaluated (if the pointing direction falls within the cut-off radius).

The sky variation of the effective beam solid angle and the ellipticity of the best-fit Gaussian to the effective beam at *HEALPix*  $N_{\text{side}} = 16$  pixel centers are shown for 100 GHz in Fig. 15. The effective beam is less elliptical near the ecliptic poles, where more scanning angles symmetrize the beam.

The mean and RMS variation of the effective beam solid angle across the sky for each HFI map are presented in Table 3.



**Fig. 15.** The effective beam solid angle (upper panel) and the best-fit Gaussian ellipticity (lower panel) of the 100 GHz effective beam across the sky in Galactic coordinates.

#### 4.1. Effective Beam Window Functions

The multipole space window function of one (or two) given observed map(s) is defined, in the absence of instrumental noise and other systematics, as the ratio of the ensemble averaged auto- (or cross-) power spectrum of the map(s) to the true theoretical sky power spectrum

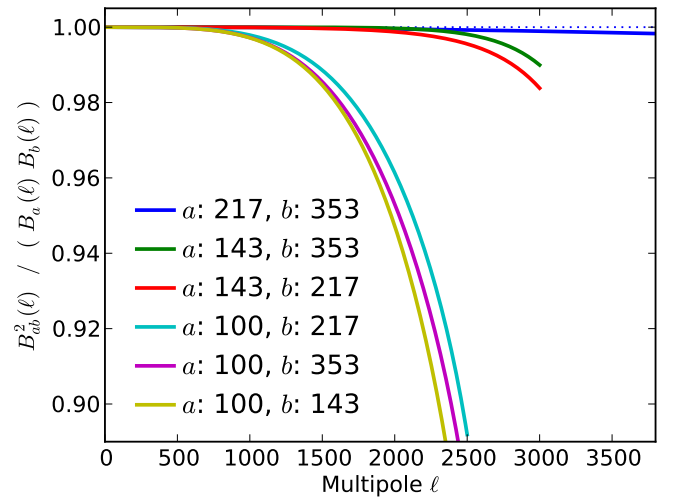
$$W_{\ell}^{\text{eff}} = \langle C_{\ell}^{\text{obs}} \rangle / C_{\ell}^{\text{sky}}. \quad (15)$$

It must account for the azimuthal asymmetry of the scan history and the beam profile. This is done in the HFI data processing pipeline using the harmonic space method Quickbeam (described in Appendix E.2) which allows a quick determination of the nominal effective beam window functions and of their

Monte Carlo based error eigenmodes (Section 6) for all auto and cross spectra pairs of HFI detectors, the error determination being computationally intractable with FEBeCop.

In the FEBeCoP approach, many (approximately 1000) random realisations of the CMB sky are generated starting from a given fiducial power spectrum  $C_{\ell}^{\text{in}}$ . For each beam model, the maps are convolved with the pre-computed effective beams, and the pseudo-power spectra  $\tilde{C}_{\ell}^{\text{conv}}$  of the resulting maps are computed and corrected by the mode coupling kernel matrix  $M$  for a given sky mask:  $C_{\ell}^{\text{obs}} = M_{\ell\ell'}^{-1} \tilde{C}_{\ell'}^{\text{conv}}$ . The Monte Carlo average of kernel-corrected power spectra compared to the input power spectrum then gives the effective beam window function (Eq. 15, with  $C_{\ell}^{\text{in}}$  replacing  $C_{\ell}^{\text{sky}}$ ).

In addition, another harmonic space method (FICSBe11; Appendix E.1) was also tested and all three methods give consistent results for the nominal window functions at 100–353 GHz (see Fig. E.1).



**Fig. 16.** Ratios of the cross-beam window functions  $B_{ab}^2(\ell)$  to the product of the respective auto-beam window functions  $B_a(\ell)B_b(\ell)$  for maps at 100, 143, 217 and 353 GHz, illustrating Eq. 16.

For two different maps obtained with different detectors or combination of detectors  $X$  and  $Y$ , because of the optical beam non-circularity and *Planck*'s scanning strategy, the cross-beam window function is not the geometrical mean of the respective auto-beam window functions

$$W^{XY}(\ell) \neq (W^{XX}(\ell)W^{YY}(\ell))^{1/2} \quad \text{if } X \neq Y, \quad (16)$$

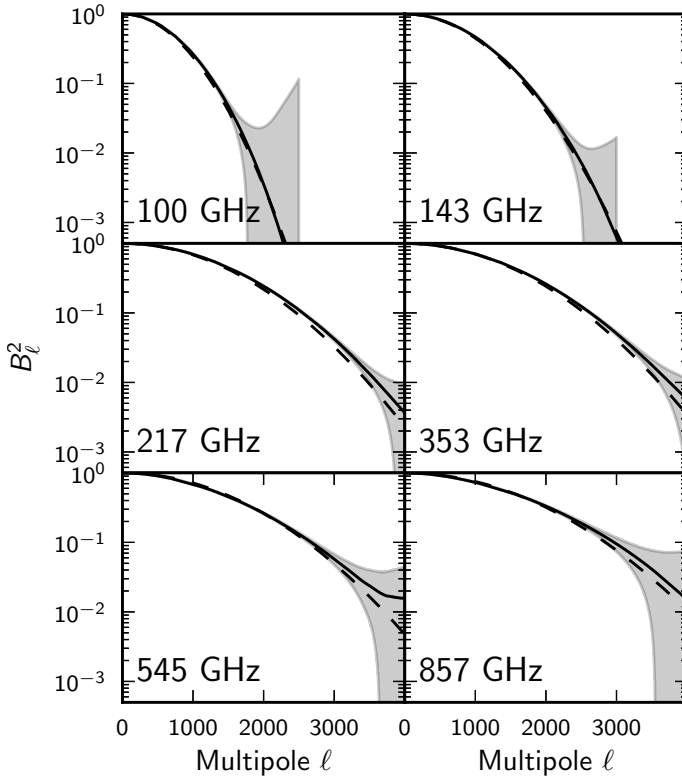
as illustrated in Fig. 16, while of course  $W^{XY} = W^{YX}$  for any  $X$  and  $Y$ .

The effective beam window functions for the 2013 maps are shown in Fig. 17. Variations in the effective beam window function from place to place on the sky are significant; the published window functions have been appropriately weighted for the analysis of the nominal mission on the full sky. Analyses requiring effective beam data for more restricted data ranges or for particular regions of the sky should refer to the specialized tools provided in Planck Collaboration ES (2013).



**Table 3.** The mean values of effective beam parameters for each HFI frequency. The error in the solid angle  $\sigma_\Omega$  comes from the scanning beam error budget. The spatial variation  $\Delta\Omega$  is the RMS variation of the solid angle across the sky. Two values are reported for the FWHM; the first is the FWHM of the Gaussian whose solid angle is equivalent to that of the effective beams. The second in parenthesis is the mean best-fit Gaussian.  $\Omega_1$  and  $\Omega_2$  are the solid angles contained within a ring of 1 and 2 FWHM respectively (Planck Collaboration XXVIII 2013). The ellipticity  $\epsilon$  is the ratio of the major to minor axis of the best fit Gaussian, averaged over the full sky.  $\Delta\epsilon$  is the RMS variability of the sky of the ellipticity.

Band	$\Omega$ [arcmin <sup>2</sup> ]	$\sigma_\Omega$ [arcmin <sup>2</sup> ]	$\Delta\Omega$ [arcmin <sup>2</sup> ]	FWHM [arcmin]	$\Omega_1$ [arcmin <sup>2</sup> ]	$\Omega_2$ [arcmin <sup>2</sup> ]	$\epsilon$	$\Delta\epsilon$
100	105.78	0.55	0.31	9.66 (9.65)	100.83	105.78	1.186	0.023
143	59.95	0.08	0.25	7.27 (7.25)	56.81	59.95	1.036	0.009
217	28.45	0.03	0.27	5.01 (4.99)	26.44	28.43	1.177	0.030
353	26.71	0.02	0.25	4.86 (4.82)	24.83	26.65	1.147	0.028
545	26.53	0.03	0.34	4.84 (4.68)	24.29	26.30	1.161	0.036
857	24.24	0.03	0.19	4.63 (4.33)	22.65	23.99	1.393	0.076



**Fig. 17.** Effective beam window functions (solid lines) for each HFI frequency. The shaded region shows the  $\pm 1\sigma$  error envelope. Dashed lines show the effective beam window function for Gaussian beams with Full-width at Half-Maximum (FWHM) 9.65, 7.25, 4.99, 4.82, 4.68, and 4.32 for 100, 143, 217, 353, 545 and 857 GHz respectively.

## 5. Uncertainties and Robustness

Ensembles of simulated planetary observations are used to propagate noise and other systematic effects in the time-ordered data into errors in the beam reconstruction. These simulations are also used to estimate bias in the reconstruction of the beam by comparing the ensemble average beam with the input beam.

To assess the completeness of the statistical and systematic noise model, the consistency of the beam reconstruction derived from different planetary observations is measured against corresponding Monte Carlo ensembles. The MC-derived beam statistics, including both the bias and the correlation structure of the

errors, have been found to be somewhat sensitive to the near lobe structure that is included in the beam used as an input to the simulations. An investigation of this effect is ongoing.

In addition, several sources of systematic error that can potentially impact the beam determination, but are not included in the current simulation pipeline, have been investigated. The most significant of these are the beam colour correction and distortion due to ADC nonlinearity. These errors are estimated separately and found to be small in comparison to the error bars estimated in the eigenmode analysis described in Section 6.

### 5.1. Simulation of planet observations

The bias and uncertainty in the scanning beam are determined using ensembles of simulated planet observations. The simulation pipeline uses the LevelS *Planck* simulation code (Reinecke et al. 2006) to generate simulations of the first two observations of Mars and the first three observations of Jupiter and Saturn for each bolometer. This pipeline is used to generate 100 simulations for each bolometer at 353 GHz, 545 GHz and 857 GHz, 200 at 143 GHz and 217 GHz, and 400 at 100 GHz. Each simulation is reconstructed into a beam model using the identical procedure and software as the real data.

The components of the simulations are as follows:

1. The scanning beams used as input to the simulations are those derived from the joint Saturn/Jupiter data. As shown in Appendix B, the reconstruction bias depends more on the beam representation than the exact input beam used in a simulation.
2. The *Planck* spacecraft pointing and the Horizons ephemerides are used to calculate the pointing relative to the planets for the simulation. An additional random 2.5 RMS per sample pointing error is added in both the in-scan and cross-scan directions with a power spectral density given by the pointing error estimate, consistent with the estimated error in the spacecraft pointing (see Sec. 4, and Fig. 7 of Planck Collaboration VI (2013)). Error in the beam centroid determination is not simulated.
3. Detector noise is generated in the timeline by a random realization of Gaussian noise with a power spectral density as reported in Planck Collaboration VI (2013).

For a small number of the simulations, cosmic ray glitches are added to the simulation with the energy spectrum and rate measured in the data (Planck Collaboration X 2013), and the deglitching procedure from the standard pipeline is applied to

detect samples contaminated by glitch transients and to subtract the long tails (Planck Collaboration VI 2013).

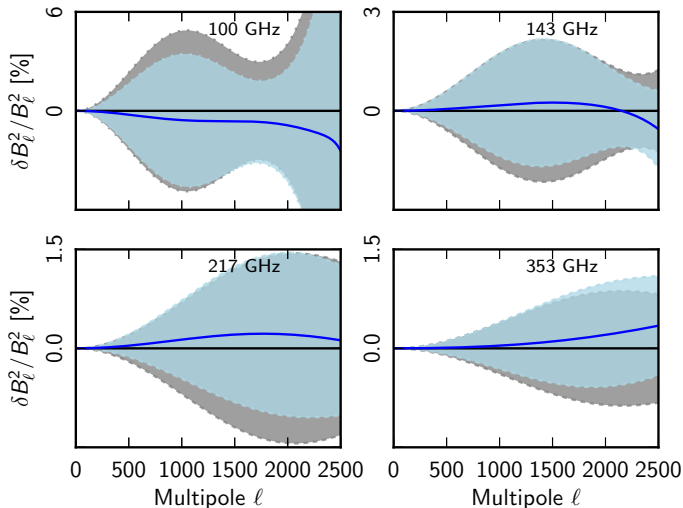
Each simulation in the ensemble provides an estimate of the scanning beam, which is then used as input to Quickbeam (Appendix E.2) to estimate an effective beam window function (EBWF). The resulting ensemble of EBWFs are then used to compute the bias and errors on the EBWF derived from the data; the mean of the ensemble provides a measure of the reconstruction bias, and the distribution of the ensemble gives the uncertainty. The majority of the RMS of the ensemble can be captured with a small number of eigenmodes (Sec. 6).

This procedure allows for the direct determination of the EBWF and associated errors for each of the detector cross-correlations input to the angular power spectrum likelihood, described in Planck Collaboration XV (2013).

## 5.2. Absolute consistency: comparison of systematics against simulations

### 5.2.1. Seasonal Consistency

One important test of the consistency of the scanning beam measurement is the stability over time, as measured in different seasons and on different objects over the course of the mission. The difference of the scanning beam window function between the first two observations of Mars is shown in Fig. 18. The residuals are well within the estimated uncertainty that is derived from the simulation ensemble for 100–353 GHz. Due to the sparse cross-scan sampling, the B-spline beam representation does not converge for a single planetary observation; for this test the Gauss-Hermite (GH) formalism is used.



**Fig. 18.** The difference between the scanning beam window functions (calculated using the Gauss-Hermite formalism) as measured on the first two observations of Mars for a single detector at four HFI frequencies. The lines give the variance-weighted average of the differences of each detector’s window function normalized to the variance-weighted average window function, at each frequency as labeled.

### 5.2.2. Time variability of planet flux density

Mars is known to have diurnal variability at HFI’s frequency of observation due to the non-uniformity of the surface albedo<sup>5</sup>. A single detector scans Mars on the time scale of a few hours, during which the brightness temperature of Mars can vary by several percent. Additionally, the Mars planetary disk area varies by several percent during an observation as it moves relative to *Planck*. To assess the impact of Mars variability on the scanning beam determination, GH representations of the beam are derived for each bolometer with and without a model for the diurnal variability of Mars. These results are indistinguishable using  $\chi^2$  test for goodness of fit.

### 5.2.3. Beam colour correction

The scanning beams are measured using planets, whose spectral energy distribution (SED) roughly follows the Rayleigh-Jeans spectrum. However, the beam window functions from these measurements are used to correct the angular power spectra of CMB anisotropies that is characterized by a very different spectrum; one that is falling in power as a function of frequency relative to a Rayleigh-Jeans spectrum across the HFI bands.

Physical optics simulations, using the GRASP software<sup>6</sup>, are used to investigate this effect. For each HFI channel from 100–353 GHz, monochromatic simulations are generated at five frequencies across each band using the pre-launch telescope model (Maffei et al. 2010; Tauber et al. 2010). The solid angle of these simulated beams varies across the band, due to diffraction and focusing effects. For 100–217 GHz, the beam size comes to a minimum near the band center, while at 353 GHz the beam size rises with frequency.

No attempt is made to colour-correct the planet-derived window functions because a telescope solution has not yet been determined that agrees with the measured solid angles. Spot checks at 143 and 353 GHz with a defocused telescope model improve agreement between the data and the model but does not change the trend of solid angle with frequency across the band. The investigation of these effects suggests that numerical models can bound the uncertainty but cannot reliably predict a bias. Rayleigh-Jeans-weighted average and CMB anisotropy-weighted average beams are produced and used to compute an effective beam window function (blue curves in Fig. 19). The largest bias results at 353 GHz. For the frequencies 100, 143, and 217 GHz however, the band average effect is less than 0.1 % across the entire multipole range used in the CMB likelihood.

The beam solid angle also varies as a function of source SED; the GRASP simulations constrain the size of the beam solid angle colour correction from a  $\nu^2$  source SED (like the planets) to the IRAS convention  $\nu^{-1}$ . At 545 and 857 GHz, the GRASP models of Murphy et al. (2010) provide a measure of the effect that is found to be significant effect at 353 GHz, but not at the other frequencies, at the level of a few tenths of a percent (Table 2).

### 5.2.4. ADC nonlinearity

Nonlinearity in the analog to digital converters (ADC) in the HFI readout electronics mainly manifests as an apparent gain drift

<sup>5</sup> <http://www.lesia.obspm.fr/perso/emmanuel-lellouch/mars/>

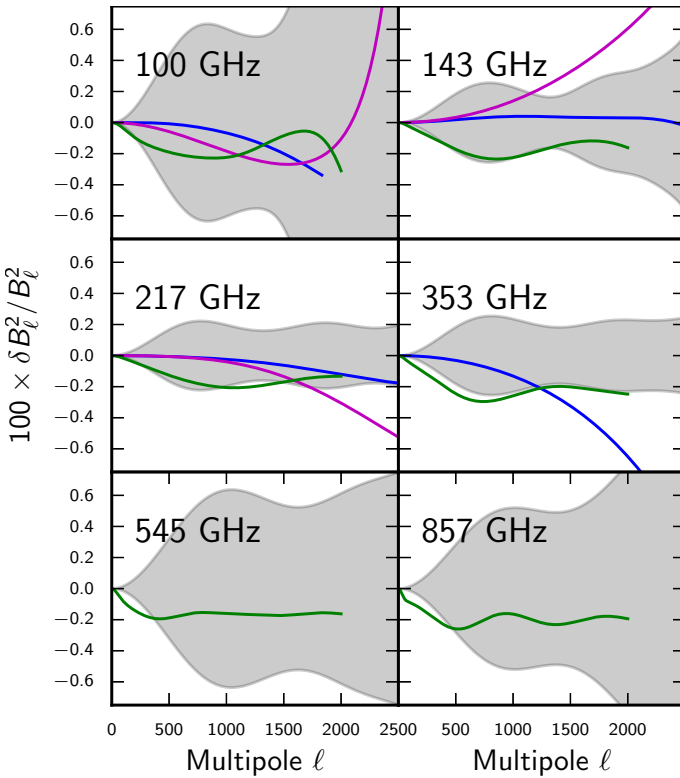
<sup>6</sup> TICRA, <http://www.ticra.com>

(Planck Collaboration VI 2013; Planck Collaboration X 2013), however the measured beam shapes are also biased by the effect.

Correcting the ADC nonlinearity relies on a model that predicts which ADC codes contribute to each data sample. The presence of large signal gradients such as a planet, or pickup from the  $^4\text{He}$ -JT cooler drive make the model difficult. The model for correcting every detector is still under development.

A model of the behaviour of the ADCs is used to apply non-linearity to simulated Mars observations. The B-spline scanning beams reconstructed from these simulations predict biases that are typically under 2 % at  $\ell \leq 2000$ , less than the RMS error (see the magenta curves in Fig. 19 for simulated bias of the 100 through 353 GHz channels).

Using the brighter planets in future *Planck* main beam models will tend to reduce the effect, as the higher signal amplitudes sample a broader range of the ADC, tending to average down the resulting bias (Mather et al. 1993).



**Fig. 19.** An estimate of known biases in the effective beam window function compared to the RMS statistical error (gray shaded region) for each HFI frequency band. Green is the bias due to near sidelobes, blue is the colour-correction bias, and magenta shows an upper limit on the effect of ADC nonlinearity.

### 5.2.5. Pointing errors

While the simulated planet observations account for random pointing errors, pointing drifts remain at the level of a few arcseconds per pointing period in the co-scan and cross-scan directions common to all detectors (Planck Collaboration I 2013; Planck Collaboration VI 2013). These have the effect of widening the beam. Even in the worst case, if remaining errors are Gaussian-distributed with a  $2''.5$  residual, the window function  $B_\ell^2$  is 0.2 % biased at multipole  $\ell = 3000$ . Since this is a very

small effect relative to the other beam errors, it is considered negligible.

### 5.2.6. Glitches

The HFI data are affected by transient signals due to interactions with high energy particles. The planet simulation tools allow the addition of a random population of glitches to simulated Mars observations with a realistic rate and energy spectrum (Planck Collaboration X 2013), testing the performance of the deglitching algorithm near planet signals and the effects of undetected low energy glitches in the channel with the highest glitch rate at each frequency band.

The RMS of the noise increases at most by 20 % in the bolometer with the highest glitch rate, but more typically less than 10 % and the reconstruction bias changes by a negligible amount. The effects are small enough that they are not included in the error budget.

### 5.3. Relative consistency: window function ratios vs. spectral ratios

The CMB sky itself allows an additional, and statistically powerful, check on the relative consistency (but not the absolute accuracy) of the effective beam window functions within a frequency band. See Fig. 33, and the associated discussion in Section 7.3 of Planck Collaboration VI (2013), showing the self-consistency of the window functions at a level better than 0.4 %, across the full range of multipoles employed in the cosmological parameter estimation.

## 6. Total error budget

The distribution of beam solid angles reconstructed from simulated planet reconstructions provides the statistical error budget for the beam solid angles (Table 2). Other systematic effects are small in comparison.

The uncertainty in the effective beam window function is determined with the distribution of window functions computed from the simulated beams. These errors are highly correlated in multipole space and we find that they can be fully described by a small number of eigenmodes and their covariance matrix (Appendix G.1 and G.2) which can be retrieved, together with the nominal beam window functions, from Planck Collaboration ES (2013) and the *Planck* Legacy Archive<sup>7</sup>. These simulations also allow us to determine the bias induced by the beam reconstruction pipeline, and correct the final beam window functions from it (Appendix G.3).

Tolerancing studies have been performed to probe the impact of assumptions regarding the near sidelobe response of the beam that is used as input to the simulations. These studies, which are currently underway, suggest the potential that the Monte Carlo ensembles used to derive the error eigenmodes may not capture aspects of the bias and the correlation structure of the errors. A visual summary of the total error budget, including the impact of the near sidelobe response, is provided in Fig. 19. For the initial data release a conservative scaling of the MC-derived beam errors, a factor of 2.7 in power, is applied in order to accommodate the maximum extent of the bias that is allowable given the signal to noise ratio of the Jupiter and Saturn data.

<sup>7</sup> [http://www.sciops.esa.int/index.php?project=planck&page=Planck\\_Legacy\\_Archive](http://www.sciops.esa.int/index.php?project=planck&page=Planck_Legacy_Archive)

## 7. Conclusion

A combination of Jupiter and Saturn observations, survey difference maps, and Checkout and Performance Verification (CPV) phase data is used to derive the bolometer/readout electronics time response transfer function. This transfer function is deconvolved from the HFI time-ordered data. Residuals can be detected as long tails stretching up to  $6^\circ$  from compact sources, but are at a level less than  $10^{-4}$  of the beam peak, and so are insignificant for the scanning beams.

The effective beams and window functions are estimated for all HFI detectors using a scanning beam derived from a combination of the first two seasons of Mars observations. The effective beam products account for the partial symmetrization of the scanning beam that results from the scan strategy. The FEBeCoP algorithm produces effective beams in real space, while the Quickbeam method is used to produce the effective beam window functions and errors in harmonic space.

The final error budget for each effective beam window function (both auto- and cross-beams) is well-described by five eigenmodes for each beam and a correlation matrix of eigenvalues. The error parameters are estimated with an ensemble of simulated Mars observations. The simulations are based on random realizations of noise and pointing errors.

No significant time variation of the scanning beam or the time response is found. Cross-power window functions are also produced that describe the beam filtering effects in cross-correlations between independent HFI maps.

The high signal to noise of the Jupiter and Saturn data limit the contribution of the near sidelobe response (between  $30'$  and  $5^\circ$  of the beam centroid) to the total beam solid angle to less than 0.2 % at 100 to 217 GHz. This portion of the beam, which is beyond the signal to noise of the Mars data, is not fully represented in the beam simulations. The Monte Carlo derived error amplitudes are scaled by a factor of 2.7 to account for the contribution of the near sidelobe response to the beam window function.

Far sidelobes contribute negligibly to the window function, but may potentially impact the primary calibration and result in pickup from bright Galactic sources. Improved physical optics models for the far sidelobes will be forthcoming for future releases.

The impact of nonlinearity in the analog to digital converter, the sensitivity of beam shape to the spectral intensity of the source and residual cosmic ray transients are found to be insignificant sources of systematic error.

Knowledge of the beam window functions allows *Planck* HFI to extrapolate the dipole calibration over more than three orders of magnitude in angular scale. For the current data release, beam errors are subdominant to noise, foreground marginalization and sample variance in cosmological parameter estimation. Future *Planck* data releases will fully exploit all of the available planetary data and create wide-field beam maps, allowing an even more precise, and accurate, measurement of the main beams and near sidelobes.

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## Appendix A: Electronics model

This appendix derives the effect of the HFI electronics filtering on the TOI. If the input signal (power) on a bolometer is

$$s_0(t) = e^{i\omega t}, \quad (\text{A.1})$$

the bolometer physical impedance can be written as:

$$s(t) = e^{i\omega t} F(\omega), \quad (\text{A.2})$$

where  $\omega$  is the angular frequency of the signal and  $F(\omega)$  is the complex intrinsic bolometer transfer function. For HFI the bolometer transfer function is modeled as the sum of 4 single pole low pass filters,

$$F(\omega) = \sum_{i=1,4} \frac{a_i}{1 + i\omega\tau_i}. \quad (\text{A.3})$$

The modulation of the signal is done with a square wave, written here as a composition of sine waves of decreasing amplitude,

$$s'(t) = e^{i\omega t} F(\omega) \sum_{k=0}^{\infty} \frac{e^{i\omega_r(2k+1)t} - e^{-i\omega_r(2k+1)t}}{2i(2k+1)}, \quad (\text{A.4})$$

where the Euler relation  $\sin x = (e^{ix} - e^{-ix})/2i$  is used, and  $\omega_r$  is the angular frequency of the square wave. The modulation frequency is  $f_{\text{mod}} = \omega_r/2\pi$  and was set to  $f_{\text{mod}} = 90.18759\text{Hz}$  in flight. This signal is then filtered by the complex electronic transfer function  $H(\omega)$ . Setting

$$\omega_k^+ = \omega + (2k+1)\omega_r$$

and

$$\omega_k^- = \omega - (2k+1)\omega_r$$

gives:

$$\Sigma(t) = \sum_{k=0}^{\infty} \frac{F(\omega)}{2i(2k+1)} \left[ H(\omega_k^+) e^{i\omega_k^+ t} - H(\omega_k^-) e^{i\omega_k^- t} \right]. \quad (\text{A.5})$$

This signal is then sampled at high frequency ( $2f_{\text{mod}}\text{NS}$ ). NS is a parameter of the HFI electronics corresponding to the number of high frequency samples in each modulation semi-period. In order to obtain an output signal sampled every  $\pi/\omega_r$  seconds, the waveform is integrated on a semi-period, as done in the HFI readout. To also include a time shift  $\Delta t$ , the integral is calculated between  $n\pi/\omega_r + \Delta t$  and  $(n+1)\pi/\omega_r + \Delta t$  (with  $T = 2\pi/\omega_r$  period of the modulation). The time shift  $\Delta t$  is encoded in the HFI electronics by the parameter  $S_{\text{phase}}$ , with the relation  $\Delta t = S_{\text{phase}}/\text{NS}/f_{\text{mod}}$ .

After integration, the  $n$ -sample of a bolometer can be written as

$$Y(t_n) = (-1)^n F(\omega) H'(\omega) e^{it_n\omega}, \quad (\text{A.6})$$

where

$$H'(\omega) = \frac{1}{2} \sum_{k=0}^{\infty} e^{-i(\frac{\pi\omega}{2\omega_r} + \omega\Delta t)} \left[ \frac{H(\omega_k^+) e^{i\omega_k^+ \Delta t}}{(2k+1)\omega_k^+} \left( 1 - e^{\frac{i\omega_k^+ \pi}{\omega_r}} \right) - \frac{H(\omega_k^-) e^{i\omega_k^- \Delta t}}{(2k+1)\omega_k^-} \left( 1 - e^{\frac{i\omega_k^- \pi}{\omega_r}} \right) \right]. \quad (\text{A.7})$$

The output signal in equation A.6 can be demodulated (thus removing the  $(-1)^n$ ) and compared to the input signal in equation A.1. The overall transfer function is composed of the



bolometer transfer function and the effective electronics transfer function,  $H'(\omega)$ ,

$$TF(\omega) = F(\omega)H'(\omega). \quad (\text{A.8})$$

The shape of  $H(\omega)$  is obtained combining low and high-pass filters with Sallen Key topologies (with their respective time constants) and accounting also for the stray capacitance low pass filter given by the bolometer impedance combined with the stray capacitance of the cables. The sequence of filters that define the electronic band-pass function  $H(\omega) = h_0 * h_1 * h_2 * h_3 * h_4 * h_5$  are listed in table A.1, with parameters listed in table A.2.

## Appendix B: Gauss-Hermite Beams

HFI's scanning beams are described by an elliptical Gaussian shape to an accuracy of 2–5 % in solid angle. A Gauss-Hermite representation of the beam uses Hermite polynomials to provide higher-order corrections to a Gaussian model (Huffenberger et al. 2010). There are fewer degrees of freedom than in a gridded beam map, allowing higher signal to noise on each mode. However, because the order of the decomposition is truncated, in practice the description is ill suited to a description of features much beyond the extent of the main beam. Larger scale features of the beam, including a beam shoulder (Ruze 1966) or the effect of the print-through of the backing structure (grating lobes), must be included separately.

The initial two-dimensional Gaussian is parametrized as

$$P(x_1, x_2) = \frac{A}{|2\pi\Sigma|^{1/2}} \exp \left[ -\frac{1}{2} \sum_{i,j=1}^2 (x_i - \bar{x}_i) \Sigma_{ij}^{-1} (x_j - \bar{x}_j) \right], \quad (\text{B.1})$$

where  $A$  is an overall amplitude,  $(x_1, x_2)$  are two-dimensional Cartesian coordinates (the pointing is projected to a flat sky),  $(\bar{x}_1, \bar{x}_2)$  are the coordinates of the beam center, and the correlation matrix is given by

$$\Sigma = \begin{pmatrix} \sigma_1^2 & \rho\sigma_1\sigma_2 \\ \rho\sigma_1\sigma_2 & \sigma_2^2 \end{pmatrix}. \quad (\text{B.2})$$

Hence, the Gaussian model parameters  $A, \bar{x}_1, \bar{x}_2, \sigma_1, \sigma_2, \rho$  are fitted. These can also be expressed in terms of the ellipticity,  $e$  (defined here as the ratio between the major and minor axes), and rotation angle  $\alpha$ , of the Gaussian ellipse.

The coefficients to the Gauss-Hermite polynomials multiplying the elliptical Gaussian are then fitted. The basis functions are defined as

$$\Phi_{n_1 n_2}(\mathbf{x}) \propto H_{n_1}(x'_1) H_{n_2}(x'_2) \exp(-\mathbf{x}' \cdot \mathbf{x}'/2), \quad (\text{B.3})$$

where  $H_n(x)$  is the order- $n$  Hermite polynomial and the primed coordinates  $\mathbf{x}'$  rotates into a system aligned with the axes of the Gaussian and scaled to the major and minor axes  $\sigma_i$  (i.e., to the principle axes of the correlation matrix  $\Sigma$ ). Having determined the elliptical Gaussian separately, the subsequent Gauss-Hermite polynomial fit is a generalized least-squares procedure, solvable by the usual matrix techniques, under the assumption of white noise. Because the full data model includes further effects such as pointing error, glitch effects, etc, a full error analysis requires a broad suite of simulations, described in Sect. 5.

## Appendix C: B-spline Beams

In this model of the scanning beam, a two-dimensional B-spline surface is fit to the time-ordered planet data. A smoothing criterion is applied during the fit to minimize the effects of high spatial frequency variations due to noise. This representation of the beam is superior to a simple two-dimensional binning of the data in its ability to capture large signal gradients.

B-splines are a linear combination of polynomials of degree  $k$  and order  $k+1$ . They are defined by the location of their control points (called *knots*) of which there are 5 for 3rd degree polynomials.

The  $k$ -degree B-spline built using the knots  $\{\lambda_i, \dots, \lambda_{i+k+1}\}$  (de Boor 1972; Cox 1972) is given by

$$P_{i,1}(x) = \begin{cases} 1, & \text{if } x \in [\lambda_i, \lambda_{i+1}] \\ 0, & \text{if } x \notin [\lambda_i, \lambda_{i+1}] \end{cases} \quad (\text{C.1})$$

with recursion relations

$$P_{i,l+1}(x) = \frac{x - \lambda_i}{\lambda_{i+l} - \lambda_i} P_{i,l}(x) + \frac{\lambda_{i+l+1} - x}{\lambda_{i+l+1} - \lambda_{i+1}} P_{i+1,l}(x). \quad (\text{C.2})$$

where the index  $l$  runs from 1 through the B-spline degree  $k$ . The B-spline knots  $\{\lambda_i, \dots, \lambda_{i+k+1}\}$  are located on a regularly spaced grid in the detector coordinate frame. At the edge of the reconstructed beam map area, 4 coincident knots are added to avoid vanishing basis functions, allowing a unique decomposition.

In the solution to the B-spline coefficients  $P_{i,l}(x)$ , a smoothing criterion is introduced as a constraint on the sum of the derivatives of the beam at each knot, motivated by the assumption that the true beam does not contain very high spatial frequencies and prevents noise from biasing the reconstruction at spatial frequencies smaller than the smoothing scale.

A smoothing criterion  $\eta$  (Dierckx 1993) is related to the the sum of the order  $k$  derivative of the beam model ( $P^k$ ) evaluated at the knot locations  $\lambda_i$ :

$$\eta = \sum_{i=1}^g \left( P^k(\lambda_{i+}) - P^k(\lambda_{i-}) \right)^2 \quad (\text{C.3})$$

where  $g$  is the total number of distinct knots and  $\lambda_{i+}$  and  $\lambda_{i-}$  are the left and right derivative of the beam model evaluated at the knot location. The smoothing criterion is introduced as an extra term in the score function  $\zeta$  in the least-squares minimization of the beam map with respect to the data,

$$\zeta = \eta + p \times \delta. \quad (\text{C.4})$$

where  $\delta$  is the usual squared difference between the data points  $y_r$  and the model  $P(x_r)$  at pointings  $x_r$ ,

$$\delta = \sum_{r=1}^m (y_r - P(x_r))^2. \quad (\text{C.5})$$

and  $p$  is a relative weighting factor for the smoothing criterion. The knot spacing and the smoothing criterion weight  $p$  are determined separately for each frequency band based on physical optics simulations and the coverage of the two Mars transits given by the scanning strategy (see Table C.1). Simulated planet observations (see Sect. 5) show that the choice of B-spline knot spacing and smoothing parameters do not significantly bias the beam reconstruction.

**Table A.1.** HFI electronics filter sequence,  $s = i\omega$ .

	Filter	Parameters	Function
0	Stray capacitance low pass filter	$\tau_{\text{stray}} = R_{\text{bolo}} C_{\text{stray}}$	$h_0 = \frac{1}{1.0 + \tau_{\text{stray}} s}$
1	Low pass filter	$R_1 = 1\text{k}\Omega$ $C_1 = 100\text{nF}$	$h_1 = \frac{2.0 + R_1 C_1 s}{2.0 (1.0 + R_1 C_1 s)}$
2	Sallen Key high pass filter	$R_2 = 51\text{k}\Omega$ $C_2 = 1\mu\text{F}$	$h_2 = \frac{(R_2 C_2 s)^2}{(1.0 + R_2 C_2 s)^2}$
3	Sign reverse with gain		$h_3 = -5.1$
4	Single pole low pass filter with gain	$R_4 = 10\text{k}\Omega$ $C_4 = 10\text{nF}$	$h_4 = \frac{1.5}{1.0 + R_4 C_4 s}$
5	Single pole high pass filter coupled to a Sallen Key low pass filter	$R_9 = 18.7\text{k}\Omega$ $R_{12} = 37.4\text{k}\Omega$ $C = 10.0\text{nF}$ $R_{78} = 510\text{k}\Omega$ $C_{18} = 1.0\mu\text{F}$ $K_3 = R_9^2 R_{78} R_{12}^2 C^2 C_{18}$ $K_2 = R_9 R_{12}^2 R_{78} C^2 + R_9^2 R_{12}^2 C^2 +$ $R_9 R_{12}^2 R_{78} C_{18} C$ $K_1 = R_9 R_{12}^2 C + R_{12} R_{78} R_9 C_{18}$	$h_5 = \frac{2.0 R_{12} R_9 R_{78} C_{18} s}{s^3 K_3 + s^2 K_2 + s K_1 + R_{12} R_{78} R_9 C_{18}}$

## Appendix D: Far Sidelobe Effects on the Effective Beam Window Function

The far sidelobes (FSL) are defined as the response of the instrument at angles  $> 5^\circ$  from the main beam centroid and can be separated into three main components (see Fig. 5 of Tauber et al. (2010)):

1. *Primary Reflector Spillover* (PR Spillover) is response of the instrument to radiation from just above the primary mirror that reflects off the secondary mirror and arrives at the feed horns. This response is nearly aligned with the spin axis of the spacecraft, and therefore scans very little of the sky on 1 minute time-scales.
2. *Secondary Reflector Direct Spillover* (SR Direct Spillover, or SRD) is the response from directly above the secondary mirror. The sidelobe peaks roughly  $10^\circ$  from the main beam, and as such scans the sky in nearly the same way as the main beam as the satellite rotates. The azimuthal extent is roughly  $30^\circ$ .
3. *Secondary Reflector Baffle Spillover* (SR Baffle Spillover, or SRB) is response from radiation reflecting off the baffles. These are difficult to model, diffuse radiation reflecting off the poorly known inner baffle surfaces. It is spread over a large fraction of the sky.

HFI's dipole calibration is performed assuming a delta-function (pencil) beam (Planck Collaboration X 2013). This leads to a bias in the calibration described by the ratio of the dipole convolved with the full-sky beam to the dipole convolved by a pencil beam,

$$\tilde{g} = g \frac{P \otimes D}{p_{\text{pencil}} \otimes D},$$

where  $\tilde{g}$  is the estimated gain,  $g$  is the true gain,  $P$  is the true full-sky beam,  $p_{\text{pencil}}$  is the assumed pencil beam, and  $D$  is the dipole. The true full-sky beam is taken to consist of three portions,

$$P = P_{\text{main}} + P_{\text{NSL}} + P_{\text{FSL}},$$

the main beam  $P_{\text{main}}$  (within  $20'$  of the centroid), the near sidelobes  $P_{\text{NSL}}$  (between  $20'$  and  $5^\circ$ ), and the far sidelobes  $P_{\text{FSL}}$  (re-

sponse further than  $5^\circ$  from the centroid).

$$P_{\text{MNSL}} = P_{\text{main}} + P_{\text{NSL}}$$

is defined as the beam within  $5^\circ$  of the centroid (the main lobe and near sidelobes). The bias in the calibration can be rewritten as

$$\tilde{g} = g \left( 1 - f_{\text{FSL}} + \frac{P_{\text{FSL}} \otimes D}{p_{\text{pencil}} \otimes D} \right), \quad (\text{D.1})$$

where  $f_{\text{FSL}}$  is the integral of the far sidelobe response relative to the full beam integral. The first term  $1 - f_{\text{FSL}}$  is due to the loss in response of the main lobe and near sidelobes to far sidelobes, while the second term represents the coupling of the dipole into the sidelobes.

For each stable pointing period the convolution of the pencil beam with the dipole is approximated by

$$p_{\text{pencil}} \otimes D \simeq \sin \theta_{\text{main}} d_{\text{pencil}}, \quad (\text{D.2})$$

where  $\theta_{\text{main}}$  is the angle between the main beam centroid and the spin axis and  $d_{\text{pencil}}$  is the dipole amplitude for the pointing period assuming a pencil beam. The components of the far sidelobes enter into Equation D.1 differently, and assuming the majority of the response to the dipole in each component comes from one direction on the sky, can be approximated as:

$$P_{\text{FSL}} \otimes D \simeq \epsilon_{\text{PR}} \sin \theta_{\text{PR}} d_{\text{pencil}} + \epsilon_{\text{SRD}} \sin \theta_{\text{SRD}} d_{\text{pencil}} + \epsilon_{\text{SRB}} \sin \theta_{\text{SRB}} d_{\text{pencil}},$$

where  $\epsilon_{\text{PR}}$ ,  $\epsilon_{\text{SRD}}$ , and  $\epsilon_{\text{SRB}}$  are the fraction of the total solid angle in the PR spillover, the SR direct spillover, and the SR baffle spillover respectively, and  $\theta_{\text{PR}}$ ,  $\theta_{\text{SRD}}$ ,  $\theta_{\text{SRB}}$  are the angles between the spin axis and the peak of the PR spillover response, the SR direct spillover response, and the SR baffle spillover response respectively. Equation D.1 then simplifies to

$$\tilde{g} \simeq g \left( 1 - f_{\text{FSL}} + \epsilon_{\text{PR}} \frac{\sin \theta_{\text{PR}}}{\sin \theta_{\text{pencil}}} + \epsilon_{\text{SRD}} \frac{\sin \theta_{\text{SRD}}}{\sin \theta_{\text{pencil}}} + \epsilon_{\text{SRB}} \frac{\sin \theta_{\text{SRB}}}{\sin \theta_{\text{pencil}}} \right), \quad (\text{D.3})$$

**Table A.2.** Parameters for LFER4 model that are deconvolved from the data.

Bolometer	$a_1$	$\tau_1$ [ms]	$a_2$	$\tau_2$ [ms]	$a_3$	$\tau_3$ [ms]	$a_4$	$\tau_4$ [ms]	$\tau_{\text{stray}}$ [ms]	$S_{\text{phase}}$
100-1a	0.392	10.0	0.534	20.9	0.0656	51.3	0.00833	572	1.59	0.00139
100-1b	0.484	10.3	0.463	19.2	0.0451	71.4	0.00808	594	1.49	0.00139
100-2a	0.474	6.84	0.421	13.6	0.0942	37.6	0.0106	346	1.32	0.00125
100-2b	0.126	5.84	0.717	15.1	0.142	35.1	0.0145	293	1.38	0.00125
100-3a	0.744	5.39	0.223	14.7	0.0262	58.6	0.00636	907	1.42	0.00125
100-3b	0.608	5.48	0.352	15.5	0.0321	63.6	0.00821	504	1.66	0.00125
100-4a	0.411	8.2	0.514	17.8	0.0581	57.9	0.0168	370	1.25	0.00125
100-4b	0.687	11.3	0.282	24.3	0.0218	62.0	0.00875	431	1.38	0.00139
143-1a	0.817	4.47	0.144	12.1	0.0293	38.7	0.0101	472	1.42	0.00125
143-1b	0.49	4.72	0.333	15.6	0.134	48.1	0.0435	270	1.49	0.00125
143-2a	0.909	4.7	0.076	17.0	0.00634	100	0.00871	363	1.48	0.00125
143-2b	0.912	5.24	0.051	16.7	0.0244	26.5	0.0123	295	1.46	0.00125
143-3a	0.681	4.19	0.273	9.56	0.0345	34.8	0.0115	317	1.45	0.00125
143-3b	0.82	4.48	0.131	13.2	0.0354	35.1	0.0133	283	1.61	0.00083
143-4a	0.914	5.69	0.072	18.9	0.00602	48.2	0.00756	225	1.59	0.00125
143-4b	0.428	6.06	0.508	6.06	0.0554	22.7	0.00882	84	1.82	0.00125
143-5	0.491	6.64	0.397	6.64	0.0962	26.4	0.0156	336	2.02	0.00139
143-6	0.518	5.51	0.409	5.51	0.0614	26.6	0.0116	314	1.53	0.00111
143-7	0.414	5.43	0.562	5.43	0.0185	44.9	0.00545	314	1.86	0.00139
217-5a	0.905	6.69	0.080	21.6	0.00585	65.8	0.00986	342	1.57	0.00111
217-5b	0.925	5.76	0.061	18.0	0.00513	65.6	0.0094	287	1.87	0.00125
217-6a	0.844	6.45	0.068	19.7	0.0737	31.6	0.0147	297	1.54	0.00125
217-6b	0.284	6.23	0.666	6.23	0.0384	24	0.0117	150	1.46	0.00111
217-7a	0.343	5.48	0.574	5.48	0.0717	23	0.0107	320	1.52	0.00139
217-7b	0.846	5.07	0.127	14.40	0.0131	47.9	0.0133	311	1.51	0.00139
217-8a	0.496	7.22	0.439	7.22	0.0521	32.5	0.0128	382	1.79	0.00111
217-8b	0.512	7.03	0.41	7.03	0.0639	27.2	0.0139	232	1.73	0.00125
217-1	0.014	3.46	0.956	3.46	0.0271	23.3	0.00359	1980	1.59	0.00111
217-2	0.978	3.52	0.014	26.1	0.00614	42	0.00194	686	1.6	0.00125
217-3	0.932	3.55	0.034	3.55	0.0292	32.4	0.00491	279	1.74	0.00125
217-4	0.658	1.35	0.32	5.55	0.0174	26.8	0.00424	473	1.71	0.00111
353-3a	0.554	7.04	0.36	7.04	0.0699	30.5	0.0163	344	1.7	0.00125
353-3b	0.219	2.68	0.671	6.95	0.0977	23.8	0.0119	289	1.57	0.00111
353-4a	0.768	4.73	0.198	9.93	0.0283	50.5	0.00628	536	1.81	0.00125
353-4b	0.684	4.54	0.224	10.8	0.0774	80	0.0149	267	1.66	0.00111
353-5a	0.767	5.96	0.159	12.4	0.0628	30.3	0.0109	357	1.56	0.00111
353-5b	0.832	6.19	0.126	11.1	0.0324	35	0.0096	397	1.66	0.00111
353-6a	0.049	1.76	0.855	6.0	0.0856	21.6	0.0105	222	1.99	0.00125
353-6b	0.829	5.61	0.127	5.61	0.0373	25.2	0.00696	360	2.28	0.00111
353-1	0.41	0.74	0.502	4.22	0.0811	17.7	0.0063	329	1.32	0.00097
353-2	0.747	3.09	0.225	7.26	0.0252	44.7	0.00267	513	1.54	0.00097
353-7	0.448	0.9	0.537	4.1	0.0122	27.3	0.00346	433	1.78	0.00125
353-8	0.718	2.23	0.261	6.08	0.0165	38	0.00408	268	1.77	0.00111
545-1	0.991	2.93	0.007	26.0	0.00139	2600	...	...	2.16	0.00111
545-2	0.985	2.77	0.013	24.0	0.00246	2800	...	...	1.87	0.00097
545-4	0.972	3.0	0.028	25.0	0.00078	2500	...	...	2.22	0.00111
857-1	0.974	3.38	0.023	25.0	0.00349	2200	...	...	1.76	0.00111
857-2	0.84	1.48	0.158	6.56	0.00249	3200	...	...	2.2	0.00125
857-3	0.36	0.04	0.627	2.4	0.0111	17	0.002	1900	1.52	0.00126
857-4	0.278	0.4	0.719	3.92	0.00162	90	0.00152	800	1.49	0.00056

From [Tauber et al. \(2010\)](#),  $\theta_{\text{pencil}} \simeq 85^\circ$ ,  $\theta_{\text{PR}} \simeq 10^\circ$ ,  $\theta_{\text{SRD}} \simeq 75^\circ$ , and  $\theta_{\text{SRB}} \simeq 45^\circ$  making the PR spillover and SR baffle spillover negligible. Equation D.3 reduces further to

$$\tilde{g} \simeq g \left( 1 - f_{\text{FSL}} + \epsilon_{\text{SRD}} \frac{\sin \theta_{\text{SRD}}}{\sin \theta_{\text{pencil}}} \right). \quad (\text{D.4})$$

SR direct spillover scans the dipole but with a slightly different amplitude since it is offset by  $10^\circ$  from the main lobe. The PR spillover does not modulate the dipole; aligned with the spin axis, the PR spillover contributes a nearly constant signal during each stable pointing period. The predicted values of the solid angle fractions are  $f_{\text{FSL}} = 3.3 \times 10^{-3}$  and  $\epsilon_{\text{SRD}} = 1.9 \times 10^{-3}$

at 100 GHz ([Tauber et al. 2010](#)), making the measured gain  $\tilde{g} \simeq 0.9985g$ .

However, the effect of the gain bias on the angular power spectrum is further reduced by corrections to the effective beam window function due to the FSL. Not including the FSL in the beam model tends to bias the window function at very low multipoles relative to high multipoles. Considering the measured sky signal at small scales  $\tilde{T}_{\text{sky}}$  as compared to the true sky  $T_{\text{sky}}$  one has

$$\tilde{T}_{\text{sky}} = \frac{S}{\tilde{g}} = \frac{P \otimes T_{\text{sky}}}{\left( 1 - f_{\text{FSL}} + \frac{P_{\text{FSL}} \otimes D}{P_{\text{pencil}} \otimes D} \right)},$$

**Table C.1.** Summary of B-spline knot spacing and smoothing criterion weight  $p$  used in the beam reconstruction.

Band [GHz]	Knot separation [arcmin]	$p$
100	1.5	10
143	1.25	10
217	1.0	10
353	1.0	$10^4$
545	0.75	$10^6$
857	0.75	$10^6$

where  $S$  is the signal measured by the bolometer. Solving for the true sky signal gives

$$P_{\text{MNSL}} \otimes T_{\text{sky}} = \left(1 - f_{\text{FSL}} + \frac{P_{\text{FSL}} \otimes D}{P_{\text{pencil}} \otimes D}\right) \tilde{T}_{\text{sky}} - P_{\text{FSL}} \otimes T_{\text{sky}}.$$

Considering that  $P_{\text{MNSL}} \otimes T_{\text{sky}} \simeq (1 - f_{\text{FSL}})T_{\text{sky}}$ ,

$$T_{\text{sky}} \simeq \left(1 + \frac{P_{\text{FSL}} \otimes D}{P_{\text{pencil}} \otimes D} \frac{1}{1 - f_{\text{FSL}}}\right) \tilde{T}_{\text{sky}} - \frac{P_{\text{FSL}} \otimes T_{\text{sky}}}{1 - f_{\text{FSL}}}.$$

Now also considering that  $P_{\text{MNSL}} \otimes D \simeq (1 - f_{\text{FSL}})P_{\text{pencil}} \otimes D$ , the true sky signal can be written as

$$T_{\text{sky}} \simeq \tilde{T}_{\text{sky}} \left(1 + \frac{P_{\text{FSL}} \otimes D}{P_{\text{MNSL}} \otimes D} - \frac{P_{\text{FSL}} \otimes T_{\text{sky}}}{P_{\text{MNSL}} \otimes T_{\text{sky}}} \frac{T_{\text{sky}}}{\tilde{T}_{\text{sky}}}\right),$$

or

$$T_{\text{sky}} = (1 + \phi_D - \phi_{\text{sky}}) \tilde{T}_{\text{sky}} \quad (\text{D.5})$$

where the second order correction term  $T_{\text{sky}}/\tilde{T}_{\text{sky}} \simeq 1$  is dropped, and the following factors are defined:

$$\phi_D = \frac{P_{\text{FSL}} \otimes D}{P_{\text{pencil}} \otimes D}$$

and

$$\phi_{\text{sky}} = \frac{P_{\text{FSL}} \otimes T_{\text{sky}}}{P_{\text{pencil}} \otimes T_{\text{sky}}}$$

$\phi_{\text{sky}}$  represents the relative pickup of anisotropy in the sidelobe beam as compared to the main beam and near sidelobes. The response of the FSL to CMB anisotropy is negligible, but Galactic response may not be. The PR spillover contributes only a constant value per pointing period because it is not modulated with the scan. Only the SR direct spillover enters into the formula. Since the SR direct spillover is nearly aligned with the main beam, Galactic signal is not picked up into the CMB anisotropy except close to the Galactic plane. So for foreground-clean regions of the sky  $\phi_{\text{sky}} \ll f_{\text{FSL}}$ .

$\phi_D$  is the bias due to the ratio of dipole response in the far sidelobes to dipole response in the main beam. Again the PR spillover contributes only an offset per pointing period which is removed by the destriping algorithm, so we are left with the SR direct spillover and SR baffle spillover. Applying the same approximation as in Equation D.2 gives

$$\phi_D \simeq \epsilon_{\text{SRD}} \frac{\sin \theta_{\text{SRD}}}{\sin \theta_{\text{pencil}}} + \epsilon_{\text{SRB}} \frac{\sin \theta_{\text{SRB}}}{\sin \theta_{\text{pencil}}},$$

and Equation D.5 becomes

$$T_{\text{sky}} \simeq \left(1 + \epsilon_{\text{SRD}} \frac{\sin \theta_{\text{SRD}}}{\sin \theta_{\text{pencil}}} + \epsilon_{\text{SRB}} \frac{\sin \theta_{\text{SRB}}}{\sin \theta_{\text{pencil}}}\right) \tilde{T}_{\text{sky}}. \quad (\text{D.6})$$

This result implies that the effective beam window function should be corrected in a way that tends to cancel the gain bias (Equation D.4), and the response to CMB anisotropy is to first order unaffected.

Simulations of the sky scanned with far sidelobe physical optics model (Planck Collaboration XIV 2013; Planck Collaboration VI 2013) confirm this.

## Appendix E: Harmonic Space Computation of the Effective Beam Window Function

Two harmonic space techniques (FICSBe11 and Quickbeam) developed independently but closely related in their formalism, have been used to compute the effective beam window functions. They provide a valuable cross-check of the pixel based results obtained with FEBeCoP (Fig. 2) and their low computational requirements allowed fast calculation of the window function errors through the processing of Monte Carlo simulations of planet observations.

### E.1. FICSBe11

FICSBe11 is a harmonic space method for computing the effective beam window function directly from the scanning beam and the scan history. The steps of this method are:

1. The statistics of the orientation of each detector  $d$  within each map pixel  $p$  is computed first, and only once for a given observation campaign:

$$w_s^d(\mathbf{r}_p) = \sum_j e^{is\psi_j} \quad (\text{E.1})$$

where  $\psi_j$  is the orientation of the detector with respect to the local meridian during the measurement  $j$  occurring in the direction  $\mathbf{r}_p$ . Note that the  $s = 0$  moment is simply the hit count map. The orientation hit moments are computed up to degree  $s = 4$ . At the same time, the first two moments of the distribution of samples within each pixel (ie, the center of mass and moments of inertia) are computed and stored on disc.

2. The scanning beam map of each detector  $d$  is transformed into spherical harmonics:

$$b_{\ell s}^d = \int d\mathbf{r} B_d(\mathbf{r}) Y_{\ell s}(\mathbf{r}), \quad (\text{E.2})$$

where  $B_d(\mathbf{r})$  is the beam map centered on the North pole, and the  $Y_{\ell s}(\mathbf{r})$  are the spherical harmonic basis functions. Higher  $s$  indices describe higher degrees of departure from azimuthal symmetry and, for HFI beams, the coefficients  $b_{\ell s}^d$  are decreasing functions of  $s$  at most multipoles considered. It also appears that, for  $\ell < 3000$ , the coefficients with  $|s| > 4$  account for much less than 1 % of the beam solid angle. Spot checks where window functions are computed with  $|s| \leq 6$  show a difference of less than  $10^{-4}$  for  $\ell < 2000$  at 100GHz and for  $\ell < 3000$  at 143 and 217GHz. For these reasons, only modes with  $|s| \leq 4$  are considered in the present analysis. Armitage-Caplan & Wandelt (2009) reached a similar conclusion in their deconvolution of LFI beams.

3. For a given CMB sky realization  $t$  described by its spherical harmonics coefficients  $a_{\ell m} = \int d\mathbf{r} t(\mathbf{r}) Y_{\ell m}(\mathbf{r})$ , the  $b_{\ell s}^d$  coefficients computed above are used to generate  $s$ -spin weighted maps,

$$m_s^d(\mathbf{r}) = \sum_{\ell m} b_{\ell s}^d a_{\ell m} Y_{\ell m}(\mathbf{r}) \quad (\text{E.3})$$



as well as the first and second order derivatives, using standard *HEALPix* tools.

4. The spin weighted maps and orientation hit moments of the same order  $s$  are combined for all detectors involved, to provide an “observed” map

$$m(\mathbf{r}) = \left( \sum_d \sum_s w_s^d(\mathbf{r}) m_s^d(\mathbf{r}) \right) / \sum_d w_0^d(\mathbf{r}). \quad (\text{E.4})$$

Similarly the local spatial derivatives are combined with the location hit moments to describe the effect of the non-ideal sampling of each pixel (see Appendix F). In this combination, the respective number of hits of each detector in each pixel is considered, as well as the weighting (generally proportional to the inverse noise variance) applied to each detector in order to minimize the final noise.

5. The power spectrum of this map can then be computed, and compared to the input CMB power spectrum to estimate the effective beam window function over the whole sky, or over a given region of the sky.

Monte Carlo (MC) simulations in which the sky realizations are changed can be performed by repeating steps 3, 4 and 5. The impact of beam model uncertainties can be studied by including step 2 in the MC simulations.

## E.2. Quickbeam

Decomposing the scanning beam into harmonic coefficients  $B_{\ell m}$ , each time-ordered information (TOI) sample can be modeled as (neglecting the contribution from instrumental noise, which is independent of beam asymmetry)

$$T_i = \sum_{\ell m s} e^{-i s \alpha_i} B_{\ell s} \tilde{T}_{\ell m s} Y_{\ell m}(\theta_i, \phi_i), \quad (\text{E.5})$$

where the TOI samples are indexed by  $i$ , and  $\tilde{T}_{\ell m}$  is the underlying sky signal. The spin spherical harmonic  ${}_s Y_{\ell m}$  rotates the scanning beam to the pointing location  $(\theta, \phi)$ , while the  $e^{-i s \alpha_i}$  factor gives it the correct orientation. Equation (E.5) may be evaluated using techniques developed for convolution in Wandelt & Gorski (2001) and Prezeau & Reinecke (2010)<sup>8</sup>, although manipulating a TOI-sized object is necessarily slow.

On the small angular scales comparable to the size of the beam, it is a good approximation to assume that the procedure of map making from TOI samples is essentially a process of binning:

$$T(p) = \sum_{i \in p} T_i / H(p), \quad (\text{E.6})$$

where  $H(p)$  is the total number of hits in pixel  $\hat{n}$ .

Given a normalized, rescaled harmonic transform of the beam  $B_{\ell m}$ , sky multipoles  $\tilde{T}_{\ell m}$  and a scan history object  $w(\hat{n}, s)$  given by

$$w(\hat{n}, s) = \sum_{j \in p} e^{i s \alpha_j} / H(\hat{n}) \quad (\text{E.7})$$

where the sum is over all hits  $j$  of pixel  $p$  at location  $\hat{n}_p$ , and  $\alpha_j$  is the scan angle for observation  $j$ . The harmonic transform of this scan-strategy object is given by

$${}_s w_{LM} = \int d^2 \hat{n}_s Y_{LM}^*(\hat{n}) w(\hat{n}, s). \quad (\text{E.8})$$

The beam-convolved observation is then given by

$$\tilde{T}(\hat{n}) = \sum_{s \ell m} w(\hat{n}, -s) B_{\ell s} T_{\ell m s} Y_{\ell m}(\hat{n}). \quad (\text{E.9})$$

Taking the ensemble average of the pseudo- $C_\ell$  power spectrum of these  $T_{\ell m}$  gives (Hanson et al. 2010; Hinshaw et al. 2007)

$$\tilde{C}_L^{TT} = \sum_{SS'} \sum_{\ell_1 \ell_2} \frac{(2\ell_1 + 1)(2\ell_2 + 1)}{4\pi} {}_{(-s-s')} \mathcal{W}_{\ell_1} B_{\ell_2 S} B_{\ell_2 S'}^* C_{\ell_2}^{TT} \times \begin{pmatrix} \ell_1 & \ell_2 & L \\ s & -s & 0 \end{pmatrix} \begin{pmatrix} \ell_1 & \ell_2 & L \\ s' & -s' & 0 \end{pmatrix} \quad (\text{E.10})$$

where

$${}_{(ss')} \mathcal{W}_L = \frac{1}{2L + 1} \sum_M {}_s w_{LM S'} w_{LM}^* \quad (\text{E.11})$$

is a cross-power spectrum of scan history objects. Note that the  $w(n, s)$  used here can also incorporate a position dependent weighting to optimize the pseudo- $C_\ell$  estimate, such as inverse-noise or a mask— the equations are unchanged. Writing the pseudo- $C_\ell$  in position space (following Dvorkin & Smith (2009)) with Wigner-d matrices gives

$$\tilde{C}_L^{TT} = \frac{1}{8\pi} \sum_{SS'} \int_{-1}^1 dz d_{00}^L(z) \times \left[ \sum_{\ell_1} d_{-s-s'}^{\ell_1}(z) {}_{(-s-s')} \mathcal{W}_{\ell_1} (2\ell_1 + 1) \right] \times \left[ \sum_{\ell_2} d_{ss'}^{\ell_2}(z) B_{\ell_2 S} B_{\ell_2 S'}^* C_{\ell_2}^{TT} (2\ell_2 + 1) \right]. \quad (\text{E.12})$$

This integral can be implemented exactly using Gauss-Legendre quadrature, with a cost of  $O(\ell_{\max}^2 s_{\max}^2)$ . For simplicity, we’ve written all the equations here for the auto-spectrum of a single detector, but the generalization to a map made by adding several detectors with different weightings is straightforward. The cost to compute all of the necessary terms exactly in that case becomes  $O(\ell_{\max}^2 s_{\max}^2 N_{\text{det}}^2)$ .

On the flat-sky, beam convolution is multiplication in Fourier space by a beam rotated onto the scan direction. Multiple hits with different scan directions are incorporated by averaging (as the scan history objects above encapsulate).

A scan strategy which is fairly smooth across the sky is nearly equivalent to observing many independent flat-sky patches at high  $L$ . There is a fairly good approximation to the beam convolved pseudo-power spectrum which is essentially a flat-sky approximation. In the limit that  $L \gg \ell_1$ , with  $C_{\ell_2}$  and  $B_{\ell_2}$  is a slowly-varying function in  $\ell_2$ , and using the equality

$$\sum_{\ell_2} (2\ell_2 + 1) \begin{pmatrix} \ell_1 & \ell_2 & L \\ s & -s & 0 \end{pmatrix} \begin{pmatrix} \ell_1 & \ell_2 & L \\ s' & -s' & 0 \end{pmatrix} = \delta_{ss'}, \quad (\text{E.13})$$

the pseudo- $C_\ell$  sum above can be approximated as

$$\tilde{C}_L^{TT} = C_L^{TT} \sum_M \left\langle |w(\hat{n}_p, M)|^2 \right\rangle_p |B_{LM}|^2, \quad (\text{E.14})$$

where the average  $\langle \rangle_p$  is taken over the full sky. It is illustrative to consider two limits of this equation: for a “raster” scan strategy in which each pixel is observed with the same direction:

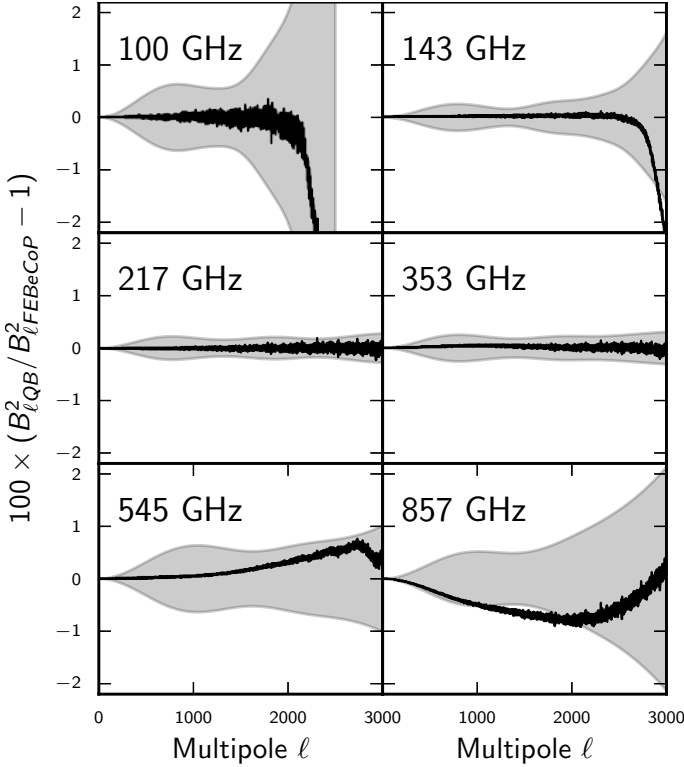
$$\left\langle |w(\hat{n}, M)|^2 \right\rangle_p = 1, \quad (\text{E.15})$$

<sup>8</sup> This approach is implemented in Level S.

and the predicted transfer function is just the power spectrum of the beam. For a “best-case” scan strategy, in which each pixel is observed many times with many different orientation angles,

$$\langle |w(\hat{n}, M)|^2 \rangle_p = \delta_{M0}, \quad (\text{E.16})$$

and the transfer function is the azimuthally symmetric part of the beam. Note that this is for a full-sky observation— in the presence of a mask, the average above produces an  $f_{\text{sky}}$  factor, as expected but neglects the coupling between  $L$  multipoles (which can be calculated with the more complete equations above).



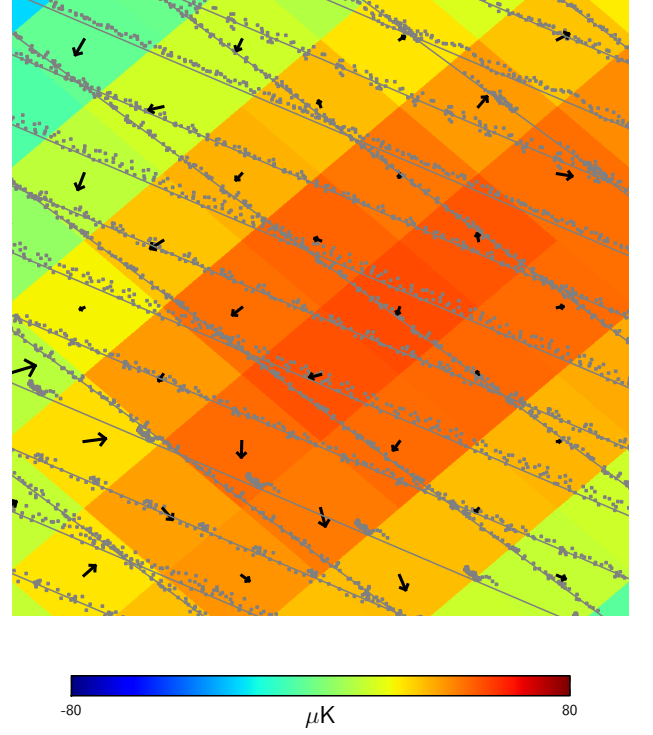
**Fig. E.1.** Difference between effective beam window functions computed with a real space method (FebeCoP) and a harmonic space method (Quickbeam). The shaded region denotes the RMS error at each multipole.

## Appendix F: Pixelization Artifacts

*Planck* maps are produced at *HEALPix* resolution 11 ( $N_{\text{side}} = 2048$ ), corresponding to pixels with a typical dimension of  $1.7'$ . With the resolution comparable to the spacing between scanning rings (Planck Collaboration I 2011) there is an uneven distribution of hits within pixels, introducing a complication in the analysis and interpretation of the *Planck* maps. A sample of the *Planck* distribution of sample hits within pixels is illustrated in Fig. F.

The three effective beam codes may also be used to simulate the effect of pixelization on the observed sky: LevelS/TotalConvolver/Conviqt ((Reinecke et al. 2006; Wandelt & Gorski 2001; Prezeau & Reinecke 2010)), FeBeCoP (Mitra et al. (2011)), and FICSBe11 (Appendix E).

For the measurement of CMB fluctuations, the effects of pixelization may be studied analytically. On the small scales relevant to pixelization, the observed CMB is smooth, both due to



**Fig. F.1.** Illustration of TOI samples near the Galactic plane (gray dots), over-plotted on a simulated CMB realization which has been convolved with a Gaussian  $7'$  FWHM beam and pixelized at ( $N_{\text{side}} = 2048$ ). Associated scanning rings (gray lines) as well as centers of mass for the hit distribution (black arrows) are also plotted.

physical damping as well as the convolution of the instrumental beam. Taylor expanding the CMB temperature about a pixel center to second order, the typical gradient amplitude is given by

$$\langle |\nabla T|^2 \rangle = \frac{1}{4\pi} \sum_{\ell} \ell(\ell+1)(2\ell+1) C_{\ell}^T W_{\ell} \approx 1 \times 10^9 \mu\text{K}^2/\text{rad}^2. \quad (\text{F.1})$$

where the approximate value is calculated for a  $\Lambda$ CDM cosmology with a  $7'$  FWHM Gaussian beam. The typical curvature of the observed temperature, on the other hand is given by

$$\langle |\nabla^2 T|^2 \rangle = \frac{1}{4\pi} \sum_{\ell} [\ell(\ell+1)]^2 (2\ell+1) C_{\ell}^T W_{\ell} \approx 7 \times 10^{14} \mu\text{K}^2/\text{rad}^4. \quad (\text{F.2})$$

On the scales relevant to the maximum displacement from the center of a  $1.7'$  pixel, the maximum displacement is  $O(1' = 3 \times 10^{-4} \text{rad})$ , and so the gradient term tends to dominate, although the curvature term is still non-negligible. For each observation of a pixel, the displacement from the pixel center can be denoted as  $d = d_{\theta} + id_{\phi}$ . The average over all hits within a pixel gives an overall deflection vector for a pixel center located at  $\hat{n}$  denoted as  $d(\hat{n})$ . This represents the center of mass of the hit distribution; Fig. F shows these average deflections using black arrows. The deflection field  $d(\hat{n})$  may be decomposed into spin-1 spherical harmonics as

$$d_{lm} = \int_{4\pi} {}_1Y_{lm}^* d(\hat{n}). \quad (\text{F.3})$$

With a second order Taylor expansion of the CMB temperature about each pixel center, it is then possible to calculate the average pseudo- $C_{\ell}$  power spectrum of the pixelized sky. This is

given by

$$C_\ell^T = [1 - \ell(\ell + 1)R^d]C_\ell^T W_\ell + \frac{1}{2} \sum_{\ell_1 \ell_2} \frac{\ell_1(\ell_1 + 1)(2\ell_1 + 1)(2\ell_2 + 1)}{4\pi} \times \begin{pmatrix} \ell_1 & \ell_2 & \ell \\ 1 & -1 & 0 \end{pmatrix}^2 C_{\ell_1}^T W_{\ell_1} [C_{\ell_2}^{d+} + (-1)^{\ell+\ell_1+\ell_2} C_{\ell_2}^{d-}], \quad (\text{F.4})$$

where  $R^d = \langle |d|^2 \rangle / 2$  is half the mean-squared deflection magnitude (averaged over hits within a pixel, as well as over pixels).  $C_\ell^{d+}$  is the sum of the gradient and curl power spectra of  $d_{\ell m}$ , and  $C_\ell^{d-}$  is the gradient spectrum minus the curl spectrum. The  $R^d$  term describes a smearing of the observed sky due to pixelization. For uniform pixel coverage of  $N_{\text{side}} = 2048$  pixels  $\langle |d|^2 \rangle^{1/2} = (2R^d)^{1/2} = 0.725'$  while, for the hit distribution of *Planck* frequency maps,  $R^d$  is within 0.2 % of this value for CMB channels, and 0.4 % for all channels. This term is therefore accurately described by the *HEALPix* pixel window function, which is derived under the assumption of uniform pixel coverage, and the resulting relative error on the beam window function is at most  $4 \times 10^{-4}$  for  $\ell \leq 3000$ .

The effect of pixelization is degenerate with that of gravitational lensing of the CMB, with the difference that it (1) acts on the beam-convolved sky, rather than the actual sky and (2) produces a curl-mode deflection field as well as a gradient mode. This is discussed further in [Planck Collaboration XVII \(2013\)](#), where the sub-pixel deflection field constitutes a potential source of bias for the measured *Planck* lensing potential. Indeed, Eq. F.4 is just a slightly modified version of the usual first order CMB lensing power spectrum ([Hu 2000](#)), [Lewis & Challinor \(2006\)](#) to accommodate curl modes.

A useful approximation to Eq. (F.4) which is derived in the unrealistic limit that the deflection vectors are uncorrelated between pixels, but in practice gives a good description of the power induced by the pixelization, is that the  $d(\hat{n})$  couples the CMB gradient into a source of noise with an effective level given by

$$\sigma^N \approx \sqrt{R^T \frac{4\pi}{N_{\text{pix}}} \langle |d(\hat{n})|^2 \rangle}, \quad (\text{F.5})$$

where the average is taken over all pixels and  $R^T$  is half the mean-squared power in the CMB gradient:

$$R^T = \frac{1}{8\pi} \sum_{\ell} \ell(\ell + 1)(2\ell + 1) \tilde{C}_\ell^T. \quad (\text{F.6})$$

For frequency-combined maps,  $\sqrt{\langle |d(\hat{n})|^2 \rangle}$  is typically on the order of 0.1, and so the induced noise  $\sigma^N$  is approximately  $2 \mu\text{K}'$ . This is small compared to the instrumental contribution, although it does not disappear when taking cross-spectra, depending on the coherence of the hit distributions of the two maps in the cross-spectra.

## Appendix G: Beam Window Function Error

### G.1. Error Eigenmodes

Consider two individual detectors or detection units (weighted sum of detectors)  $X$  and  $Y$  for which sky maps are available. Here  $X$  and  $Y$  can be the same or different. Putting aside the instrumental noise and other contingencies for the time being, the

cross- (or auto-) angular power spectrum measured of the observed maps  $C_{\text{obs}}^{XY}(\ell)$  is in *average* related to the real input signal one  $C_{\text{sky}}^{XY}(\ell)$  through

$$\langle C_{\text{obs}}^{XY}(\ell) \rangle = C_{\text{sky}}^{XY}(\ell) W_{\text{eff,true}}^{XY}(\ell) \quad (\text{G.1})$$

where  $W_{\text{eff,true}}^{XY}$  is the effective beam window function. Note that because of the optical beam non-circularity and *Planck* scanning strategy,

$$W^{XY}(\ell) \neq (W^{XX}(\ell) W^{YY}(\ell))^{1/2} \quad \text{if } X \neq Y, \quad (\text{G.2})$$

as illustrated in Fig. 16, while  $W^{XY} = W^{YX}$  for any  $X$  and  $Y$ . It also appears that in the  $\ell$  range of interest,  $W^{XY}(\ell) \geq 0$ ; therefore  $W^{XY} = (B^{XY})^2$  in analogy to what is usually done for simple (circular) beam models. In what follows, the  $XY$  pair superscript is dropped except when they are required for clarity. In most cases, scientific analyses will be conducted on a best guess  $C_{\text{est}}(\ell)$  of the sky power spectrum, in which the empirical  $C_{\text{obs}}(\ell)$  is corrected from a nominal effective window  $W_{\text{eff,nom}}(\ell)$

$$C_{\text{est}}(\ell) = C_{\text{obs}}(\ell) / W_{\text{eff,nom}}(\ell), \quad (\text{G.3})$$

therefore, in average,

$$\begin{aligned} \langle C_{\text{est}}(\ell) \rangle &= C_{\text{sky}}(\ell) W_{\text{eff,true}}(\ell) / W_{\text{eff,nom}}(\ell), \\ &= C_{\text{sky}}(\ell) (B_{\text{eff,true}}(\ell) / B_{\text{eff,nom}}(\ell))^2. \end{aligned} \quad (\text{G.4})$$

The ratio  $B_{\text{eff,true}}(\ell) / B_{\text{eff,nom}}(\ell)$  which determines the uncertainties on the angular power spectrum originating from our beam knowledge is studied out of the planet transit MC simulations described in Sect. 5. The scanning beam map determined with the B-Spline code described in Appendix C on each of these simulations is turned into an effective beam window function  $W_i(\ell)$  for  $i = 1, 2, \dots, n_{\text{MC}}$  (where  $n_{\text{MC}} = 100$  is the number of MC simulations) using the Quickbeam formalism described in Appendix E.2.

Defining the means  $B_{\text{mean}}(\ell)$  and  $W_{\text{mean}}(\ell)$  as

$$B_{\text{mean}}(\ell) = \sum_{i=1}^{n_{\text{MC}}} (W_i(\ell))^{1/2} / n_{\text{MC}} \quad (\text{G.5})$$

$$W_{\text{mean}}(\ell) = \sum_{i=1}^{n_{\text{MC}}} W_i(\ell) / n_{\text{MC}} \quad (\text{G.6})$$

one can build the matrix of the deviations around the mean

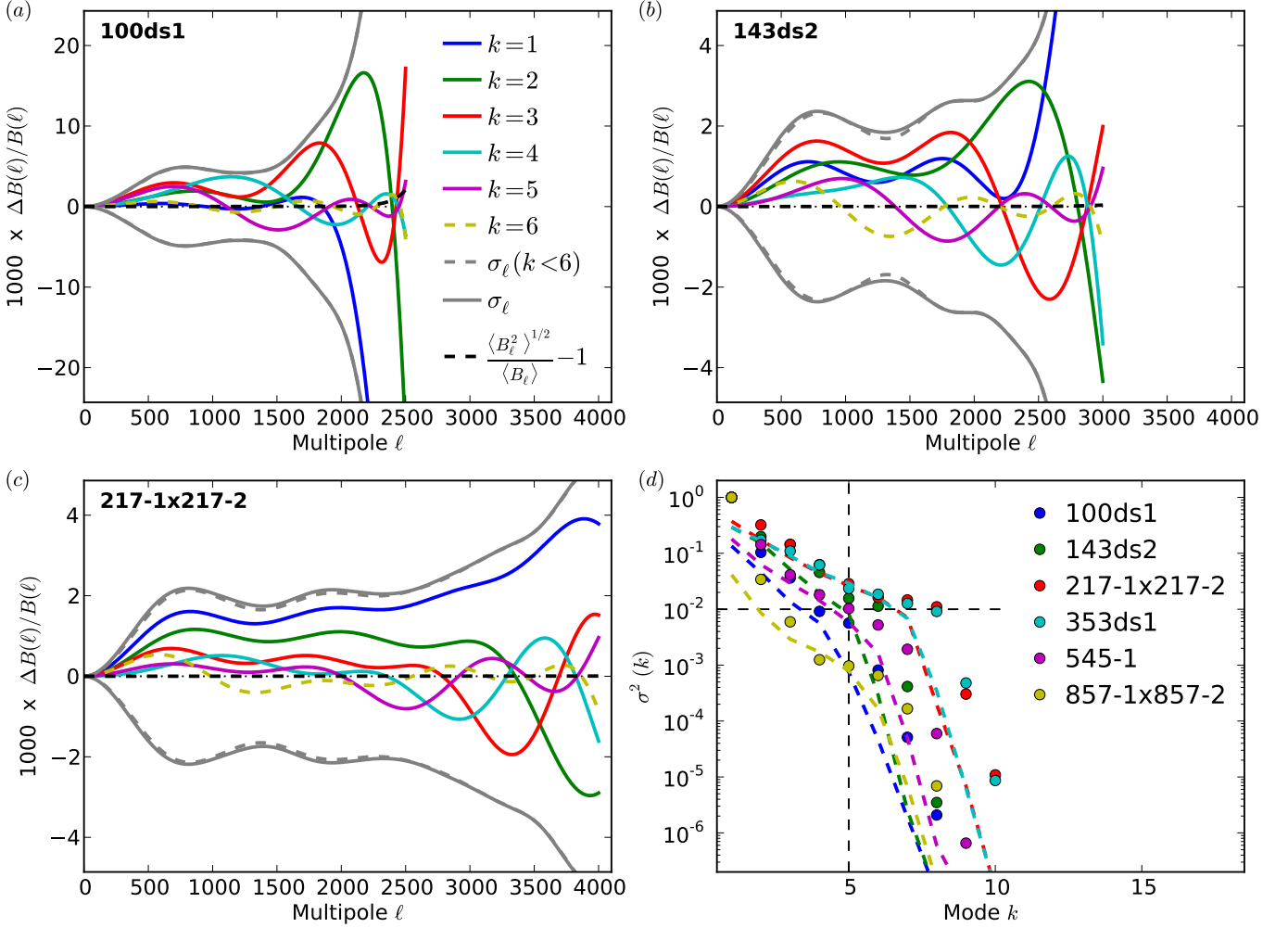
$$\Delta_i(\ell) = f_s \ln (B_i(\ell) / B_{\text{mean}}(\ell)), \quad (\text{G.7})$$

where the factor  $f_s$  has been applied. As discussed in Sect. 6,  $f_s = 2.7$ . This scaling factor is applied throughout the rest of discussion and is enclosed in the delivered products and plotted error modes.

Sect. G.3 contains a discussion of how the MC average  $B_{\text{mean}}$  and nominal beam  $B_{\text{eff,nom}}$  are related and focus here on the dispersion around the mean.

Since the relative dispersion of the simulated  $W_i(\ell)$  generally is very small (less than 1%), then  $W_{\text{mean}}(\ell) \simeq B_{\text{mean}}(\ell)^2$  to a very good approximation (as illustrated in Fig. G.1) and the matrix  $\Delta$  is well approximated by

$$\begin{aligned} \Delta_i(\ell) &\simeq 1/2 f_s \ln (W_i(\ell) / W_{\text{mean}}(\ell)), \\ &\simeq 1/2 f_s (W_i(\ell) / W_{\text{mean}}(\ell) - 1). \end{aligned} \quad (\text{G.8})$$



**Fig. G.1.** Beam window function error modes. Panels *a*, *b* and *c* show the first 6 eigenmodes defined in Eq. (G.11) for respectively the effective auto-beam 100ds1 and 143ds2 and the effective cross-beam 217-1x217-2. The first 5 modes used in the current beam error modeling are shown as solid colored curves, while the 6th mode (the first one to be ignored) appears as yellow dashes. The grey dashes show  $1\sigma$  envelope obtained by adding the first 5 modes in quadrature, while the solid grey curve is the  $1\sigma$  estimated from the simulations (therefore including all eigenmodes). The black dashes show the relative difference between  $W_{\text{mean}}^{1/2}(\ell)$  and  $B_{\text{mean}}(\ell)$  defined in Eqs. G.6 and G.5 respectively. In panel *d*, for a selection of effective beams, the colored symbols show  $(d_k/d_1)^2$  where  $d_k$  is the  $k$ -th eigenvalue of the diagonal matrix  $\mathbf{D}$  (Eq. G.12), while the colored dashes show the error made on the quadratic sum of the eigenvalues by truncating it to  $n_{\text{modes}}$ :  $1 - \sum_{k=1}^{n_{\text{modes}}} d_k^2 / \sum_{k=1}^{\infty} d_k^2$ . The vertical dashes show the current  $n_{\text{modes}} = 5$  value.

The quantity  $B(\ell)$  was preferred over  $W(\ell)$  in order to remain consistent with the usual description of the beam in map linear space, instead of quadratic space.

The statistical properties of the MC based beam window functions can be summarized in the covariance of the deviations  $\Delta$ , defined as

$$\mathbf{C} \equiv \Delta^T \Delta / (n_{\text{MC}} - 1), \quad (\text{G.9})$$

where  $\Delta$  is a matrix with  $n_{\text{MC}}$  rows and  $\ell_{\text{max}} + 1$  columns, and  $\mathbf{C}$  is a square symmetric positive semi-definite matrix with  $\ell_{\text{max}} + 1$  rows and columns. It can be diagonalized into

$$\begin{aligned} \mathbf{C} &= \mathbf{V} \mathbf{D}^2 \mathbf{V}^T / (n_{\text{MC}} - 1), \\ &= \mathbf{E}^T \mathbf{E}, \end{aligned} \quad (\text{G.10})$$

where  $\mathbf{D}$  is a diagonal matrix, with at most  $n_{\text{MC}}$  positive eigenvalues, and the eigenmodes matrix

$$\mathbf{E} \equiv \mathbf{D} \mathbf{V}^T / (n_{\text{MC}} - 1)^{1/2} \quad (\text{G.11})$$

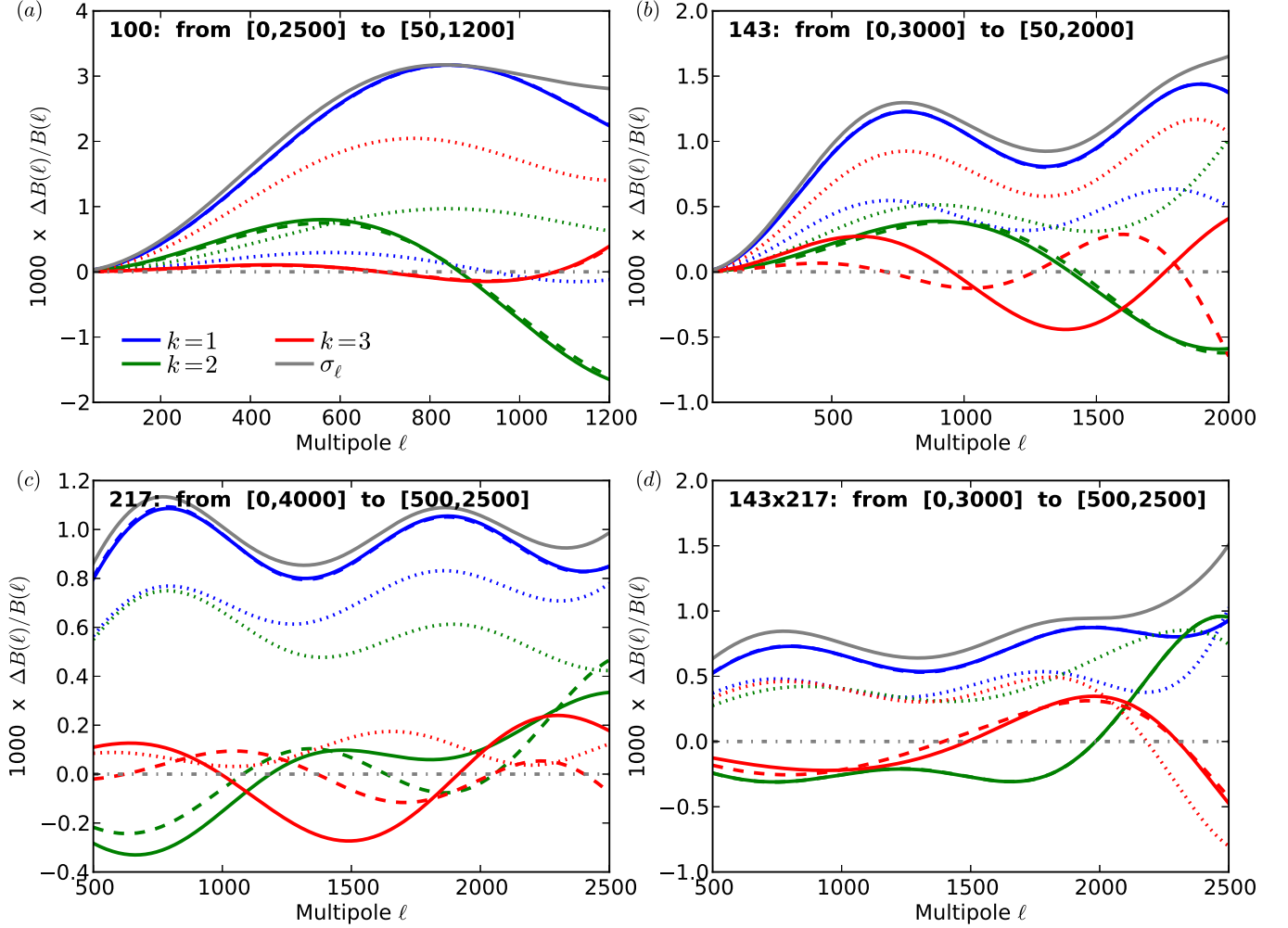
of the beam uncertainty. Alternatively, one can perform a Singular Value Decomposition (SVD) of  $\Delta$ , which reads

$$\Delta = \mathbf{M} \mathbf{D} \mathbf{V}^T \quad (\text{G.12})$$

$$= \mathbf{M} \mathbf{E} (n_{\text{MC}} - 1)^{1/2} \quad (\text{G.13})$$

where  $\mathbf{M}$  is an orthogonal  $n_{\text{MC}} \times n_{\text{MC}}$  matrix (ie,  $\mathbf{M}^T \mathbf{M} = \mathbf{I}_{n_{\text{MC}}}$ ),  $\mathbf{D}$  is a diagonal matrix with  $n_{\text{MC}}$  non-negative eigenvalues of decreasing amplitude, and  $\mathbf{V}$  is a matrix with  $\ell_{\text{max}} + 1$  rows whose  $n_{\text{MC}}$  columns are orthonormal vectors (ie,  $\mathbf{V}^T \mathbf{V} = \mathbf{I}_{n_{\text{MC}}}$ ) with  $\mathbf{I}_{n_{\text{MC}}}$  being the identity matrix of size  $n_{\text{MC}} \times n_{\text{MC}}$ . The diagonalization of the covariance matrix  $\mathbf{C}$  (Eq. G.10) has a numerical complexity scaling like  $\ell_{\text{max}}^3$ , while the SVD of  $\Delta$  (Eq. G.12) scales like  $\ell_{\text{max}} n_{\text{MC}}^2$ . Since  $n_{\text{MC}} \ll \ell_{\text{max}}$  the latter approach was preferred because it is much faster, and it naturally provides the mixing matrix  $\mathbf{M}$ . Equation (G.12) has a degeneracy on the sign of  $\mathbf{M}$  and  $\mathbf{V}$  which was lifted by con-





**Fig. G.2.** Effect of  $\ell$  truncation on beam error modes for frequency averaged beam window function at 100, 143, 217 GHz and 143x217. For clarity, only the three leading modes are shown respectively in blue, green and red, while the solid gray line shows the one  $\sigma$  standard deviation, obtained by adding *all* modes in quadrature. Dotted lines: original eigenmodes computed on a wide  $\ell$ -range. Solid lines: eigenmodes computed directly from the MC simulations on the truncated  $\ell$ -range used for cosmological analysis. Dashed lines: eigenmodes computed on the truncated  $\ell$ -range with Eqs. G.16 and G.17 starting from the first five eigenmodes for the wide range. In all four cases considered, the first leading mode on the truncated range, which dominates the error budget, is perfectly reconstructed out of the information available, while the second leading mode is well estimated in all cases except for 217 GHz.

straining the vectors of  $\mathbf{V}$  (and therefore  $\mathbf{E}$ ) to all be positive at  $l = 200$ .

It appears that most of the statistical content of  $\mathbf{\Delta}$  or  $\mathbf{C}$  is described by the first few modes  $n_{\text{modes}}$  with the largest eigenvalues, in which case the  $\mathbf{E}$  matrix is truncated to its first  $n_{\text{modes}}$  rows with little loss of information. For HFI,  $n_{\text{modes}} = 5$  is chosen, as illustrated in Fig. G.1.

The statistics of the elements of the mixing matrix  $\mathbf{M}$ , and therefore of the MC measured beam window function fluctuations, is shown in Fig. G.3 to be very close to Gaussian, justifying the current analysis in terms of a covariance matrix.

The beam uncertainty model therefore is

$$B(\ell) = B_{\text{mean}}(\ell) \exp(\mathbf{g}^T \cdot \mathbf{E})_\ell \quad (\text{G.14})$$

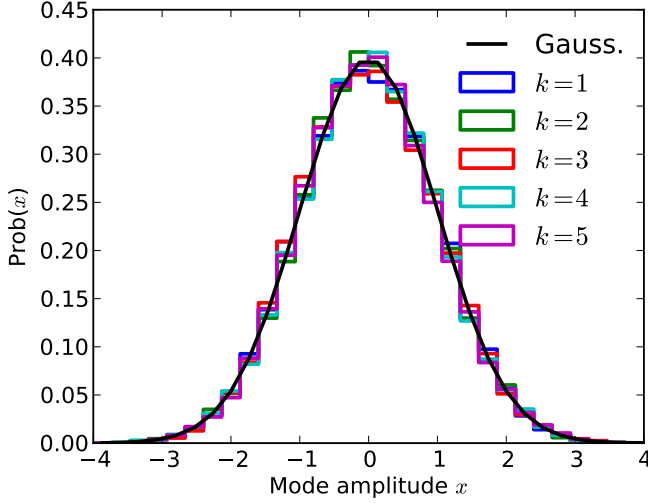
$$= B_{\text{mean}}(\ell) \exp\left(\sum_{k=1}^{n_{\text{modes}}} g_k e_k(\ell)\right) \quad (\text{G.15})$$

where  $\mathbf{g}$  is a  $n_{\text{modes}}$  element vector of independant Gaussian variates of zero mean and unit variance and  $e_k(\ell)$  is the  $k$ -th row of  $\mathbf{E}$ .

The SVD decomposition of the beam uncertainty was performed for the  $\ell$  range  $[\ell_{\text{min}}, \ell_{\text{max}}]$  with  $\ell_{\text{min}} = 0$  and  $\ell_{\text{max}}$  depending on the frequencies of the two detectors involved in the beam considered. Currently  $\ell_{\text{max}} = 2500$  when the lowest frequency is 100 GHz,  $\ell_{\text{max}} = 3000$  when that frequency is 143 GHz, and  $\ell_{\text{max}} = 4000$  at higher frequency.

If orthogonal error eigenmodes are needed for the range  $[\ell'_{\text{min}}, \ell'_{\text{max}}]$  with  $\ell'_{\text{min}} \geq \ell_{\text{min}}$  and  $\ell'_{\text{max}} \leq \ell_{\text{max}}$ , the provided  $\mathbf{E}$  must first be truncated to the new range to give the  $\mathbf{E}_t$  matrix with  $n_{\text{modes}}$  rows and  $\ell'_{\text{max}} - \ell'_{\text{min}} + 1$  columns, and then Singular Value Decomposed into

$$\mathbf{E}_t = \mathbf{R}' \cdot \mathbf{D}' \cdot \mathbf{V}'^T, \quad (\text{G.16})$$



**Fig. G.3.** Distribution of the eigenmodes determined from MC simulations, for all HFI detector sets, for the first  $n_{\text{modes}}=5$  modes, compared to a Gaussian distribution of zero mean and unit variance.

where the new set of orthogonal eigenmodes is

$$\mathbf{E}' \equiv \mathbf{D}' \cdot \mathbf{V}^T. \quad (\text{G.17})$$

This is illustrated on Fig. G.2, where are shown the eigenmodes truncated to the frequency dependent  $\ell$  ranges used in the *Planck*  $C(\ell)$  likelihood (Planck Collaboration XV 2013).

### G.2. Eigenmode Covariance

The previous approach, dedicated to the study of the uncertainty on the beam window function associated to a single pair of detectors (or maps), can be generalized to the simultaneous characterization of any number of pairs. For instance for the three disjoint pairs  $a = \{UV\}$ ,  $b = \{XY\}$  and  $c = \{ZT\}$ , one writes

$$(\Lambda^a \Lambda^b \Lambda^c) = (\mathbf{M}^a \mathbf{M}^b \mathbf{M}^c) \cdot \begin{pmatrix} \mathbf{E}^a & 0 & 0 \\ 0 & \mathbf{E}^b & 0 \\ 0 & 0 & \mathbf{E}^c \end{pmatrix}. \quad (\text{G.18})$$

and the covariance matrix reads

$$\begin{aligned} \mathbf{C}^{abc} &= (\Lambda^a \Lambda^b \Lambda^c)^T \cdot (\Lambda^a \Lambda^b \Lambda^c) \\ &= \begin{pmatrix} \mathbf{E}^a & 0 & 0 \\ 0 & \mathbf{E}^b & 0 \\ 0 & 0 & \mathbf{E}^c \end{pmatrix}^T \cdot \begin{pmatrix} \mathbf{I} & \mathbf{M}^{aT} \mathbf{M}^b & \mathbf{M}^{aT} \mathbf{M}^c \\ \mathbf{M}^{bT} \mathbf{M}^a & \mathbf{I} & \mathbf{M}^{bT} \mathbf{M}^c \\ \mathbf{M}^{cT} \mathbf{M}^a & \mathbf{M}^{cT} \mathbf{M}^b & \mathbf{I} \end{pmatrix} \cdot \begin{pmatrix} \mathbf{E}^a & 0 & 0 \\ 0 & \mathbf{E}^b & 0 \\ 0 & 0 & \mathbf{E}^c \end{pmatrix}, \\ &= \mathbf{E}^{a,b,cT} \cdot \mathbf{M}^{a,b,c} \cdot \mathbf{E}^{a,b,c}, \end{aligned} \quad (\text{G.19})$$

where  $\mathbf{M}^{a,b,c}$  is a square symmetric matrix with  $3n_{\text{modes}}$  rows, and if one denotes  $\mathbf{L}^{a,b,c}$  its Cholesky 'root' such that  $\mathbf{M}^{a,b,c} = \mathbf{L}^{a,b,c} \cdot \mathbf{L}^{a,b,cT}$ , then

$$B^a(\ell) = B_{\text{mean}}^a(\ell) \exp(\mathbf{g}^T \mathbf{L}^{a,b,c} (\mathbf{E}^a \mathbf{0} \mathbf{0}))_\ell \quad (\text{G.20})$$

$$B^b(\ell) = B_{\text{mean}}^b(\ell) \exp(\mathbf{g}^T \mathbf{L}^{a,b,c} (\mathbf{0} \mathbf{E}^b \mathbf{0}))_\ell \quad (\text{G.21})$$

$$B^c(\ell) = B_{\text{mean}}^c(\ell) \exp(\mathbf{g}^T \mathbf{L}^{a,b,c} (\mathbf{0} \mathbf{0} \mathbf{E}^c))_\ell \quad (\text{G.22})$$

where  $\mathbf{g}$  is  $3n_{\text{modes}}$  element vector of independent Gaussian deviates and is the same for Eqs. (G.20) to (G.22).

The *Planck*-HFI RIMO available at *Planck* Legacy Archive<sup>9</sup> and described in Planck Collaboration ES (2013) contains the correlation matrix  $\mathbf{M}^{a,b,c,d,\dots}$  where  $a, b, c, d, \dots$  each are a different element of the set of pairs that can be built out of the detection units available. So, for  $n_d$  detection units, the number of pairs will be  $n_d(n_d + 1)/2$  and the correlation matrix will be square and symmetric, 1-valued on its diagonal and have  $n_{\text{modes}} n_d(n_d + 1)/2$  rows and as many columns. The  $n_{\text{modes}}$  relative to the same detector pair form adjacent rows and columns in the matrix, and the order of appearance of the pairs in the matrix is specified in the header of the FITS extension containing the matrix. The nominal  $B(\ell)$  and eigenmodes  $\mathbf{E}$  are provided for each pair in a different extension.

The results above were obtained in the basis of eigen-modes provided, if one wants to obtain a beam correlated model on a different  $\ell$ -range, with the eigenmodes  $\mathbf{E}'$  defined in Eq. (G.17), then the covariance matrix becomes

$$\mathbf{C}'^{abc} = \begin{pmatrix} \mathbf{E}'^a & 0 & 0 \\ 0 & \mathbf{E}'^b & 0 \\ 0 & 0 & \mathbf{E}'^c \end{pmatrix}^T \cdot \mathbf{M}^{a,b,c} \cdot \begin{pmatrix} \mathbf{E}'^a & 0 & 0 \\ 0 & \mathbf{E}'^b & 0 \\ 0 & 0 & \mathbf{E}'^c \end{pmatrix}, \quad (\text{G.23})$$

with

$$\mathbf{M}'^{a,b,c} = \begin{pmatrix} \mathbf{R}'^a & 0 & 0 \\ 0 & \mathbf{R}'^b & 0 \\ 0 & 0 & \mathbf{R}'^c \end{pmatrix}^T \cdot \mathbf{M}^{a,b,c} \cdot \begin{pmatrix} \mathbf{R}'^a & 0 & 0 \\ 0 & \mathbf{R}'^b & 0 \\ 0 & 0 & \mathbf{R}'^c \end{pmatrix}, \quad (\text{G.24})$$

where the  $\mathbf{R}'$  matrices are obtained from the SVD in Eq. (G.16).

### G.3. Monte Carlo bias

As discussed in Sect. 3.2, the Monte Carlo average of the B-Spline reconstructed effective beam window function  $B_{\text{mean}}(\ell)$  can be different from the effective beam that would be obtained directly out of the simulation input beam map  $B_{\text{eff,in}}(\ell)$ , introducing a bias

$$1 + \varepsilon_{\text{bias}}(\ell) \equiv B_{\text{mean}}(\ell) / B_{\text{eff,in}}(\ell), \quad (\text{G.25})$$

which is interpreted as a consequence of the imperfect sampling of the beam map by the planet, the effect of the instrumental noise and pointing uncertainty and the smoothing feature of the B-spline functions. It is found that  $|\varepsilon_{\text{bias}}(\ell=500)| \leq 2 \cdot 10^{-4}$  and  $|\varepsilon_{\text{bias}}(\ell=1000)| < 5 \cdot 10^{-4}$  for all effective beams, making it smaller than the relative dispersion on the beam window function described above. It is assumed that the beam reconstruction on the real data suffers from the same bias, and its beam window function  $B_{\text{eff,raw}}(\ell)$  is corrected from it to provide the nominal beam

$$B_{\text{eff,nom}}(\ell) = B_{\text{eff,raw}}(\ell) / (1 + \varepsilon_{\text{bias}}(\ell)), \quad (\text{G.26})$$

$$= B_{\text{eff,raw}}(\ell) B_{\text{eff,in}}(\ell) / B_{\text{mean}}(\ell). \quad (\text{G.27})$$

In doing so,  $\varepsilon_{\text{bias}}$  is assumed perfectly determined by the simulations, and no error is associated with this correction.

<sup>9</sup> [http://www.sciops.esa.int/index.php?project=planck&page=Planck\\_Legacy\\_Archive](http://www.sciops.esa.int/index.php?project=planck&page=Planck_Legacy_Archive)

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